



CATALOG 2015

LAYERTEC®
OPTICAL COATINGS · OPTICS

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PRECISION OPTICS

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SELECTED SPECIAL COMPONENTS

COMPONENTS FOR OPTICAL PARAMETRIC OSCILLATORS (OPO)

Mirrors for OPOs are optimized for separation of the pump laser, signal and idler wavelengths. This application requires a broad reflection band of the signal wavelengths and a wide range of high transmission for the idler wavelengths.

Moreover, most of the optics show smooth group delay (GD) and group delay dispersion (GDD) spectra. Thus, wide tuning ranges for the signal and the idler wavelengths can be achieved. This enables the operation of OPOs with fs-pulses. Broadband output couplers are also available. Center wavelength and tuning range can be adjusted according to customer specifications.

All OPO coatings are produced by magnetron sputtering. This process guarantees that the optical parameters are environmentally stable, because the coatings are dense, free of water and adhere strongly to the substrate in spite of the extreme coating thickness of 20 – 30 μm . This makes sputtered OPO coatings ideal for application in harsh environments.

CAVITY MIRRORS FOR AOI = 0°

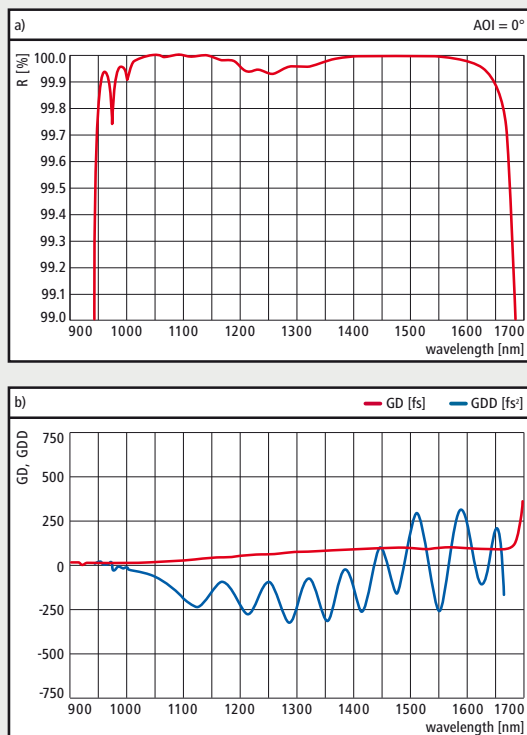


Figure 1: Reflectance, GD and GDD spectra of a broadband HR mirror for the signal wavelength: HR (0°, 1000 – 1600 nm) > 99.9 %

- a) Reflectance vs. wavelength
- b) GD and GDD vs. wavelength

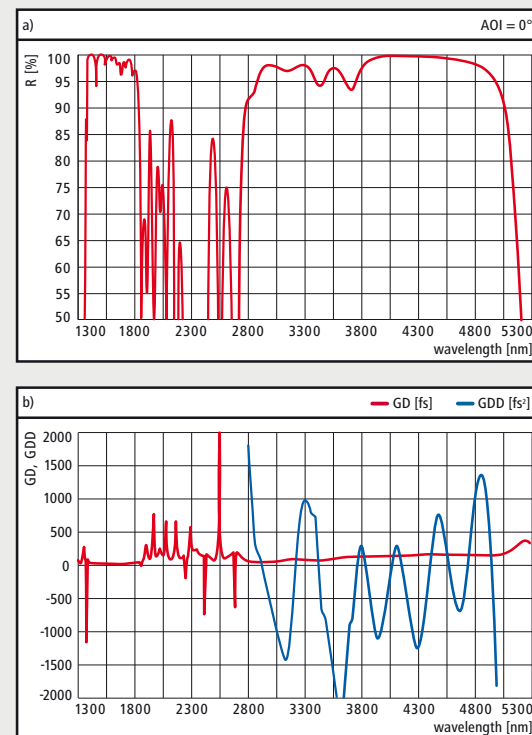
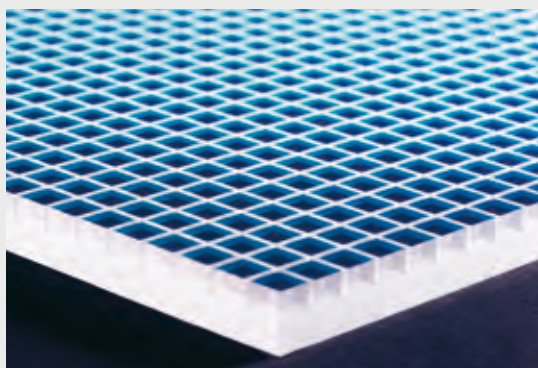


Figure 2: Reflectance, GD and GDD spectra of a dual HR mirror for the signal and idler wavelengths: HR (0°, 1400 – 1800 nm) > 96 %

- + HR (0°, 2900 – 4900 nm) > 93 %
- a) Reflectance vs. wavelength
- b) GD and GDD vs. wavelength



This dual wavelength mirror shows smooth GD spectra for signal and idler, but only the broadband mirror for the idler wavelengths is GDD optimized.

PUMP MIRRORS AND SEPARATORS AOI = 0°

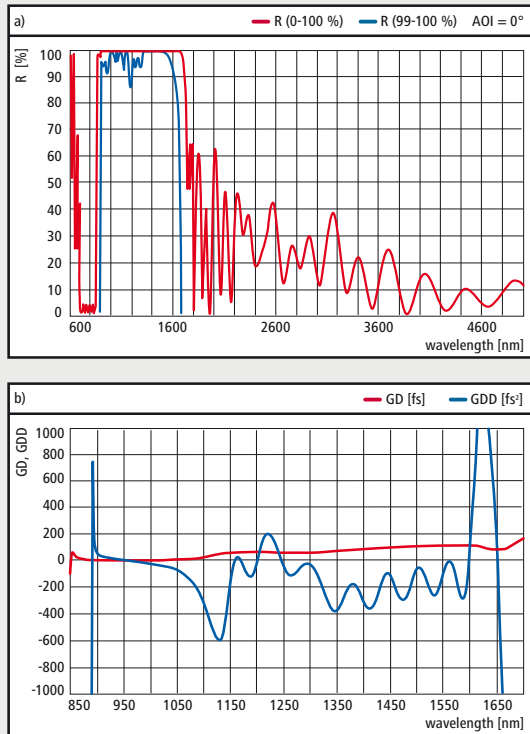


Figure 3: Reflectance, GD and GDD spectra of an OPO pump mirror
 a) Reflectance vs. wavelength
 b) GD and GDD vs. wavelength

This type of mirrors separates the pump and signal wavelengths while suppressing the idler wavelength:
 $R(0^\circ, 700 - 850 \text{ nm}) < 10\%$
 $+ HR(0^\circ, 900 - 1600 \text{ nm}) > 99.8\%$
 $+ R(0^\circ, 1800 - 5000 \text{ nm}) < 60\%$.

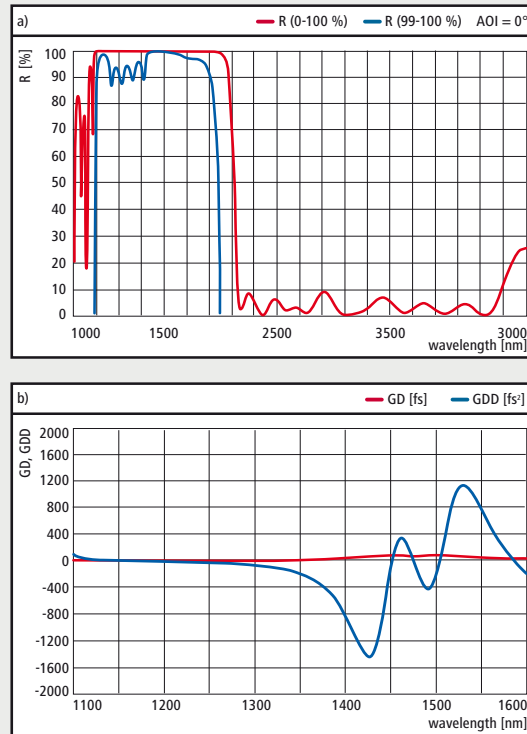


Figure 4: Reflectance, GD and GDD spectra of a separator for the signal and idler wavelengths
 a) Reflectance vs. wavelength
 b) GD and GDD vs. wavelength

- Edge filters separating signal and idler wavelengths can be used as broadband outcoupling mirrors for the idler:
 $HR(0^\circ, 1100 - 1600 \text{ nm}) > 99.8\%$ + $R(0^\circ, 1730 - 2900 \text{ nm}) < 10\%$.
- These filters can also be provided with a band of high reflectance or high transmission for the pump wavelengths or for the second harmonic of the signal wavelengths.
- We recommend undoped YAG or sapphire as substrate material if high transmission for the idler wavelengths is required.
 (see also page 21 for transmission curves)

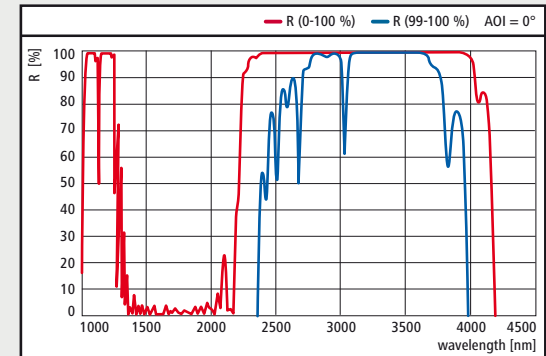


Figure 5: Reflectance spectrum of a broadband mirror for the NIR:
 $HR(0^\circ, 2300 - 4000 \text{ nm}) > 99\%$

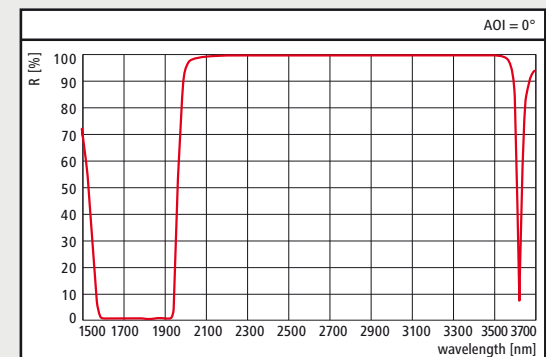


Figure 6: Reflectance spectrum of a broadband mirror for the NIR:
 $HR(0^\circ, 2050 - 3500 \text{ nm}) > 99\%$ + $HT(0^\circ, 1600 - 1930 \text{ nm})$

COMPONENTS FOR OPTICAL PARAMETRIC OSCILLATORS (OPO)

OUTPUT COUPLERS FOR AOI = 0°

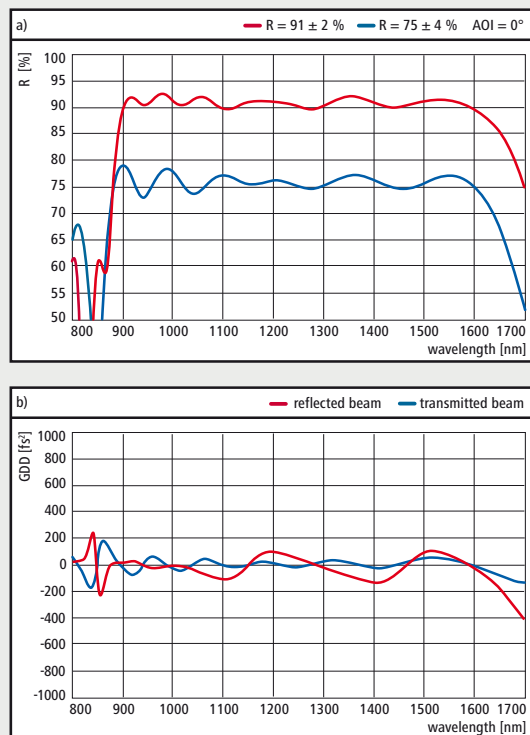


Figure 1: Reflectance and GDD spectra of different broadband output couplers for the signal wavelengths.

a) Reflectance vs. wavelength

b) GDD vs. wavelength

Please note the smooth GDD spectra. The GDD spectra shown are calculated for the 75 % output coupler, but the spectra for other reflectivity values are very similar.

BEAM SPLITTERS FOR AOI = 45°

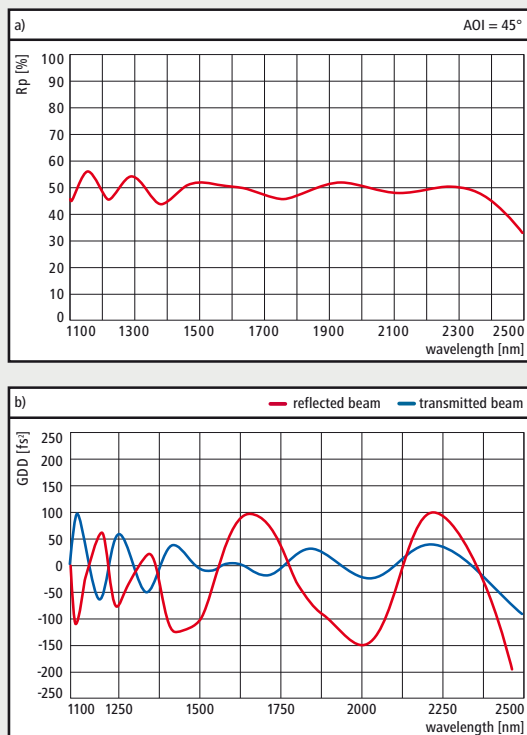


Figure 2: Reflectance and GDD spectra of a broadband beam splitter for p-polarized signal and idler radiation:

R_p (45°, 1100 – 2400 nm) = $50 \pm 5\%$

a) Reflectance vs. wavelength

b) GDD vs. wavelength

SPECIAL OUTPUT COUPLERS FOR AOI = 0°

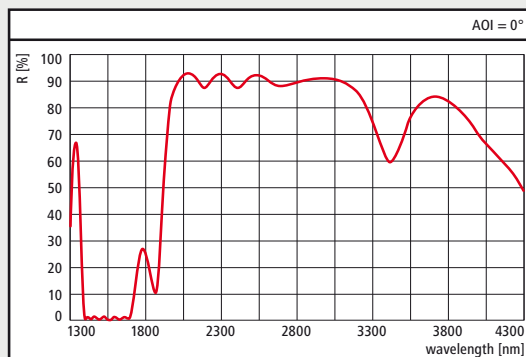


Figure 3: Reflectance spectrum of a special output coupler:

R (0°, 1400 – 1700 nm) < 3%

+ PR (0°, 2000 – 3150 nm) = $90 \pm 3\%$

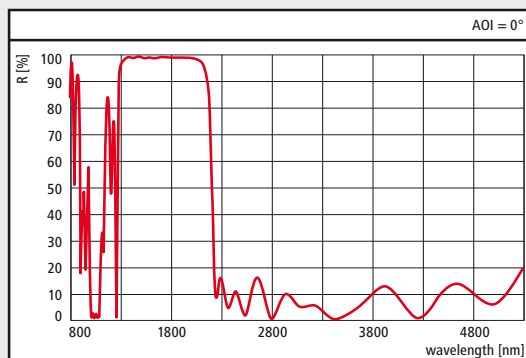


Figure 4: Reflectance spectrum of a special output coupler:

R (0°, 1000 – 1100 nm) < 3%

+ PR (0°, 1350 – 2000 nm) = $98 \pm 5\%$

+ R (0°, 2200 – 5000 nm) < 20 %

The reflectivity of output couplers and beam splitters can be adjusted according to customer specifications.

The output couplers for the signal wavelengths (fig. 3) can suppress the idler and vice versa (fig. 4). These output couplers may also have a pump window.

TURNING MIRRORS AND SEPARATORS FOR AOI = 45°

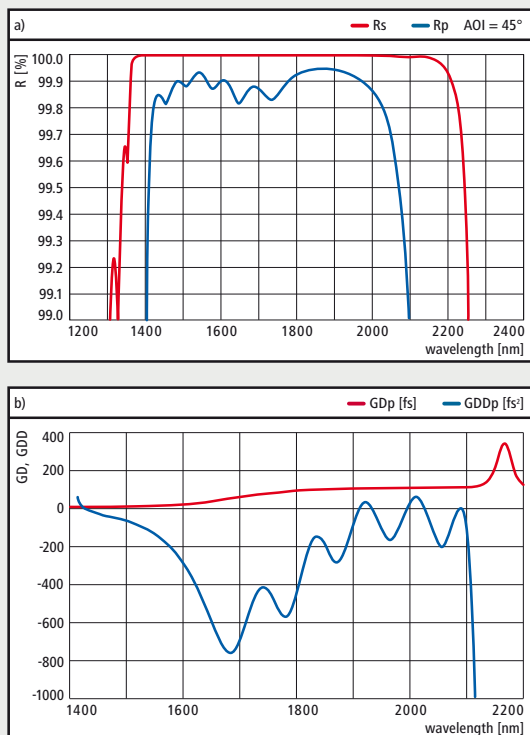


Figure 5: Reflectance, GD and GDD spectra of a turning mirror HRp (45°, 1450 – 2000 nm) > 99.8 %
a) Reflectance vs. wavelength
b) GD and GDD vs. wavelength

Turning mirrors and separators for pump wavelengths, signal and idler are key components of OPOs. On this page we present some examples of such optics. The spectral position of the reflection and transmission bands can be adjusted according to customer specifications. Please note that the GD and GDD can only be optimized for s- or p-polarization while the reflectivity is usually very high for both polarizations.

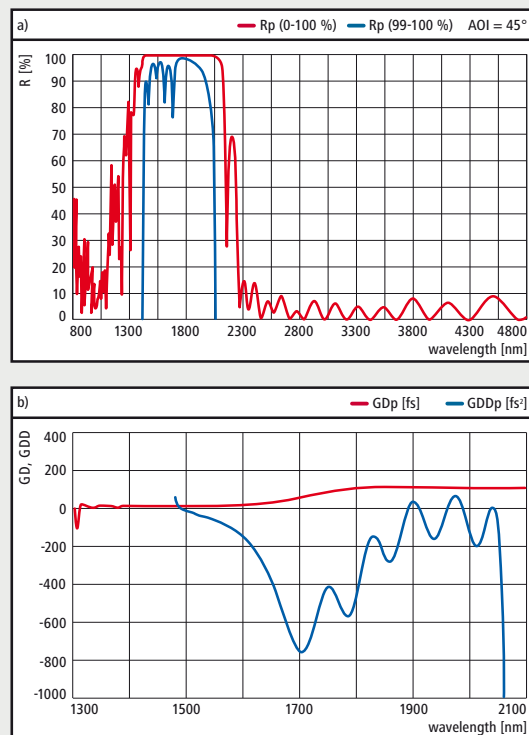


Figure 6: Reflectance, GD and GDD spectra of a separator for signal and idler
a) Reflectance vs. wavelength
b) GD and GDD vs. wavelength

A broad reflectance band for the signal wavelengths is combined with a broad transmission band for the idler:

HRp (45°, 1450 – 2000 nm) > 99.8 %
+ Rp (45°, 2350 – 4000 nm) < 10 %.

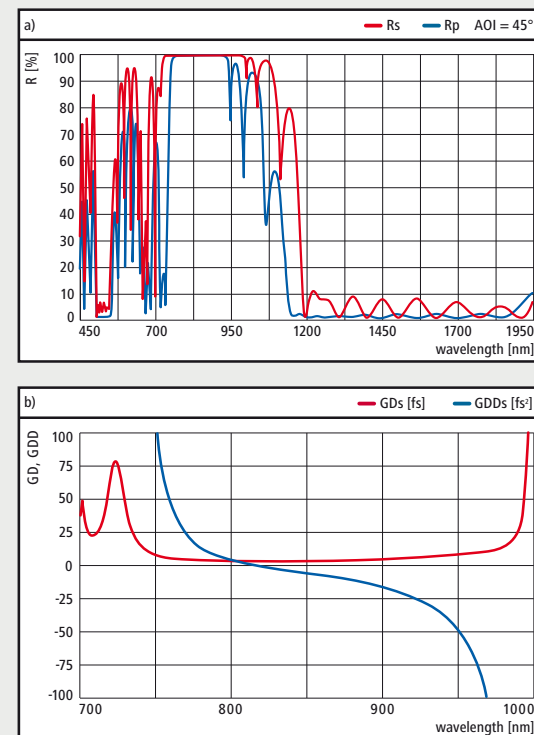


Figure 7: Reflectance, GD and GDD spectra of a separator for the signal and idler with high transmission for the pump radiation
a) Reflectance vs. wavelength
b) GD and GDD vs. wavelength

This separator can be used to couple the pump radiation into the resonator:

HRs (45°, 770 – 930 nm) > 99.8 %
+ Rp (45°, 510 – 550 nm) < 1 %
+ Rp (45°, 1160 – 1900 nm) < 10 %.

COMPONENTS FOR OPTICAL PARAMETRIC OSCILLATORS (OPO)

ULTRA BROADBAND COMPONENTS FOR AOI = 45°

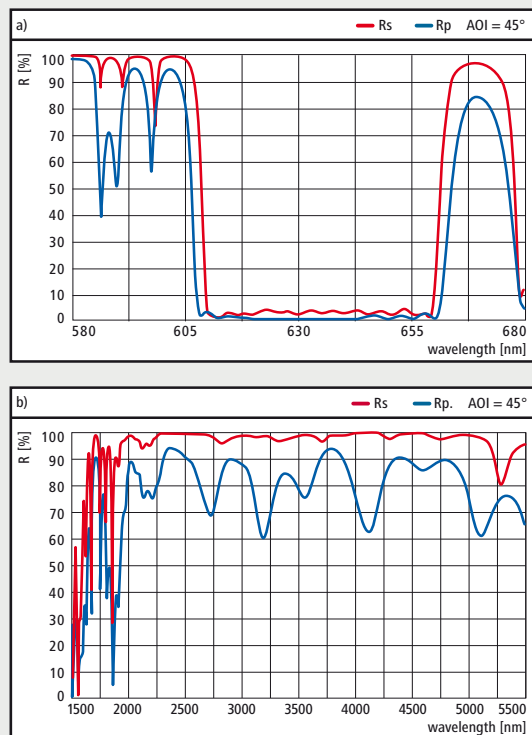


Figure 1: Reflectance spectrum of an ultra broadband beam combiner
 HRs (45°, 2000 – 5000 nm) > 98 %
 + Rp (45°, 633 nm) < 2%

This beam combiner can be used to couple an alignment laser into the beam line. Please note the very low reflectivity at 620 – 650 nm.

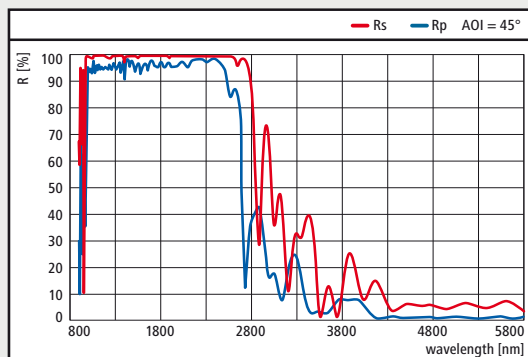


Figure 2: Reflectance spectrum of an ultra broadband separator for signal and idler wavelengths
 HRr (45°, 1000 – 2500 nm) > 98 %
 + Rr (45°, 4400 – 5000 nm) < 5 %

EDGE FILTERS FOR AOI = 45°

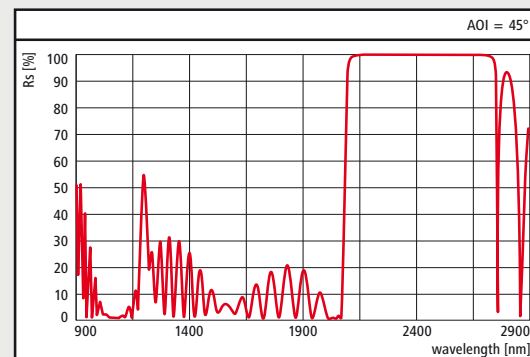


Figure 3: Reflectance spectrum of an edge filter for the idler and signal wavelength range with high transmission for the pump wavelength:
 HRs (45°, 2150 – 2700 nm) > 99.9 %
 + Rs (45°, 2000 – 2070 nm) < 10 % + Rs (45°, 1064 nm) < 1 %

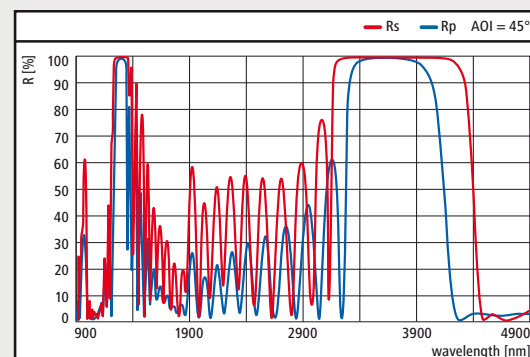


Figure 4: Reflectance spectrum of a broadband edge filter for the idler wavelength range with high transmission for the pump wavelength:
 HRs (45°, 3300 – 4200 nm) > 99.9 %
 + Rs (45°, 4500 – 4900 nm) < 6 % + Rs,p (45°, 1064 nm) < 5 %

SPECIAL MIRRORS AOI = 0°

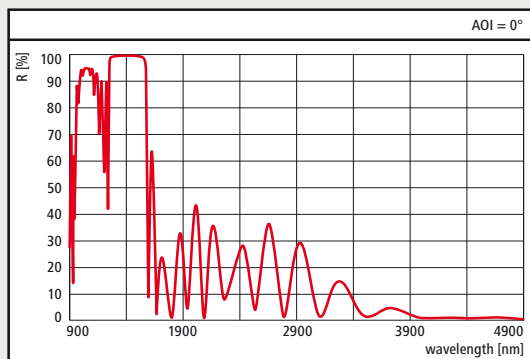


Figure 5: Reflectance spectrum of a special pump mirror:
 PR (0°, 1064 nm) = 94 ± 2 %
 + HR (0°, 1360 – 1460 nm) > 99.9 %
 + R (0°, 4000 – 4900 nm) < 3 %

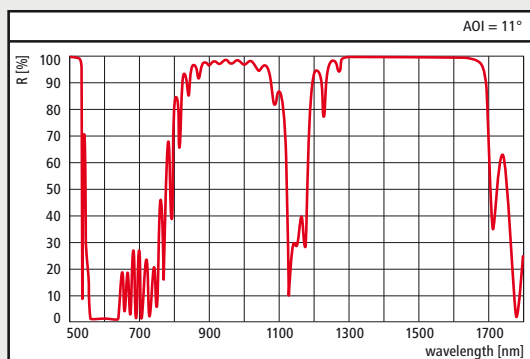


Figure 6: Reflectance spectrum of a special mirror:
 R (11°, 565 – 620 nm) < 1 %
 + PR (11°, 900 – 1000 nm) = 98 ± 0.5 %
 + HR (11°, 1280 – 1600 nm) > 99.9 %

COATINGS ON NONLINEAR OPTICAL CRYSTALS AOI = 0°

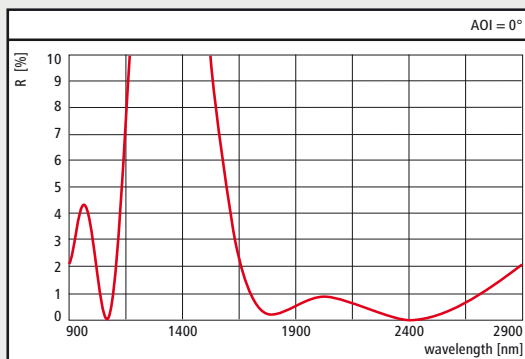


Figure 7: Reflectance spectrum of an AR coating on lithium niobate:
 R (0°, 1064 nm) < 0.5 % + R (0°, 1750 – 2750 nm) < 1 %

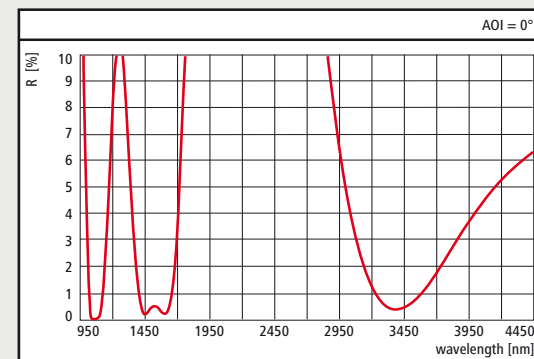


Figure 9: Reflectance spectrum of an AR coating on lithium niobate:
 R (0°, 1064 nm) < 0.5 % + R (0°, 1420 – 1640 nm) < 0.5 %
 + R (0°, 3150 – 3700 nm) < 2 %

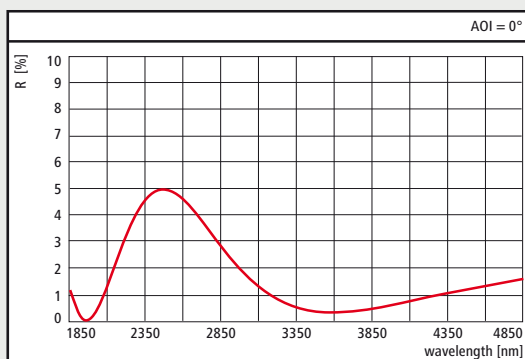


Figure 8: Reflectance spectrum of an AR coating on lithium niobate:
 R (0°, 1910 – 2030 nm) < 0.5 %
 + R (0°, 3200 – 4200 nm) < 1 %

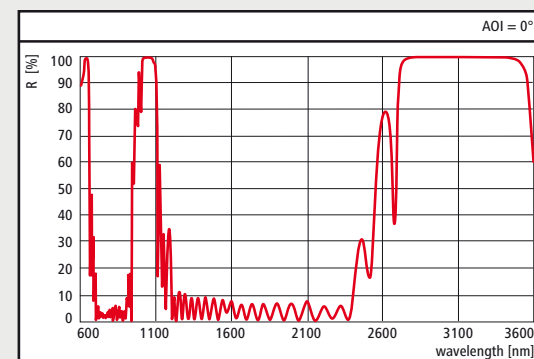


Figure 10: Reflectance spectrum of a double reflector with two regions of high transmittance on lithium niobate
 HR (0°, 1010 – 1075 + 2750 – 3450 nm) > 99.8 %
 + R (0°, 700 – 900 + 1200 – 2400 nm) < 10 %

All coatings according to customer specifications.

BROADBAND AND SCANNING MIRRORS

LAYERTEC produces broadband and scanning mirrors according to customer specifications. Full dielectric and metal-dielectric coating designs are used. In the following, we present examples which are designed for broad wavelength regions or extremely large ranges of incidence angles.

Broadband mirrors are widely used to reflect light from lasers that emit in a broad wavelength range like for example Ti:Sapphire lasers, dye lasers, or a combination of different diode lasers.

Special mirrors are also available to cover the whole visible spectrum, the near ultraviolet and considerable parts of the near infrared spectral regions. We recommend such mirrors as universal turning mirrors for nearly all types of laser diodes.

Broadband mirrors for the NIR range are especially useful for reflecting idler wavelengths of optical parametric oscillators or for special fs-applications. In combination with fused silica as a substrate material, a large blocking range from 2300 – 6000 nm can be achieved. Other NIR materials such as sapphire and YAG are possible alternatives. These materials can be used for high power applications to improve the cooling of the optics through the thermal conductivity of the substrate. This may be necessary if the absorption of water (around 2.8 μm) or of the coating material itself leads to an increase in temperature.

BROADBAND MIRRORS

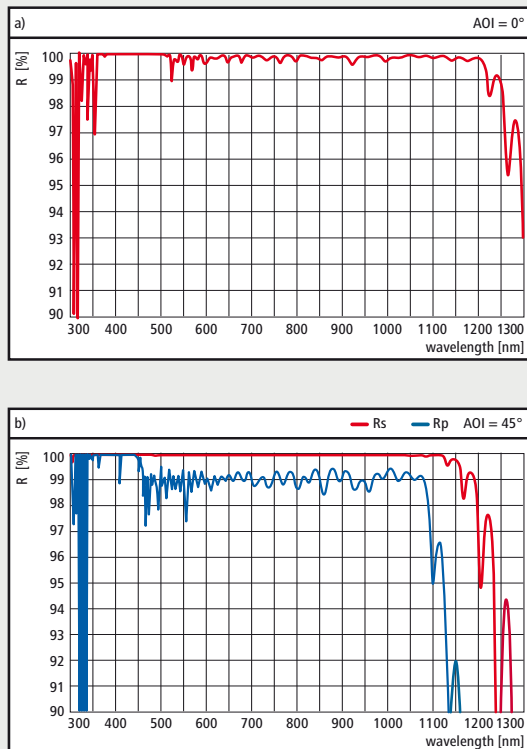


Figure 1: Reflectance spectra of an ultra broadband mirror for the NUV, VIS and NIR
 a) $R(0^\circ, 360 - 1200 \text{ nm}) > 99 \%$
 b) $R_s(45^\circ, 350 - 1150 \text{ nm}) > 99 \%$
 + $R_p(45^\circ, 350 - 1050 \text{ nm}) > 97 \%$

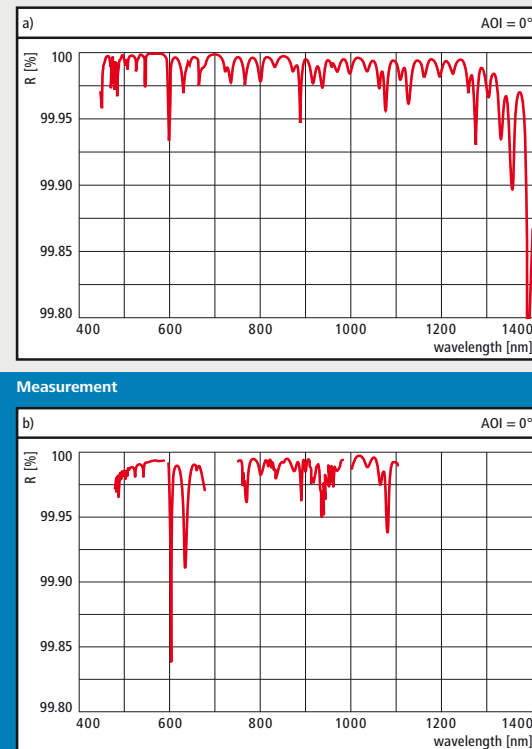


Figure 2: Reflectance spectra of a broadband mirror
 HR (0° , 400 – 1400 nm) > 99.9 %
 a) Calculated design
 b) Broadband CRD measurement

Please note the good conformity between calculation and measurement. The CRD measurements are limited by the water absorption in the 750 – 780 nm and 1200 – 1400 nm regions. For these regions, measurements in vacuum are required.

400 – 1800 nm

SCANNING MIRRORS

LAYERTEC offers scanning mirrors for high power laser applications and for special demands with respect to wavelength and angular range. Scanning mirrors are optimized for high reflectance for one wavelength or a certain wavelength region at a wide range of angles of incidence. Our coating technology provides industrial solutions for lightweight scanning mirrors and special mirrors with uncommon sizes up to 500 mm for research with cw and pulsed high power lasers.

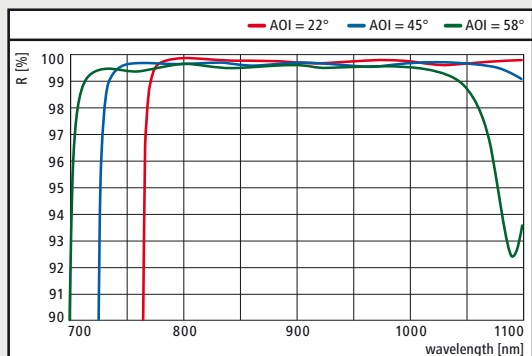
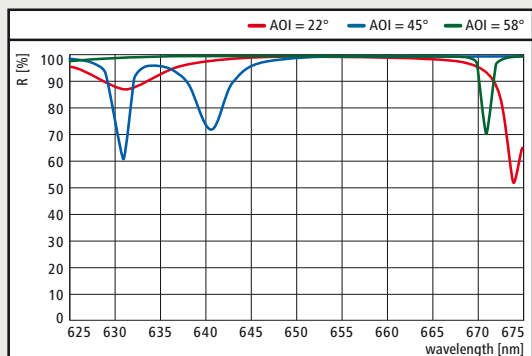


Figure 3: Reflectance spectra of a silver based scanning mirror with enhanced wavelength range for laser diodes in the NIR:
HRr (22° – 58°, 800 – 1000 nm) > 99 %
+ PRr (22° – 58°, 630 – 670 nm) > 50 %

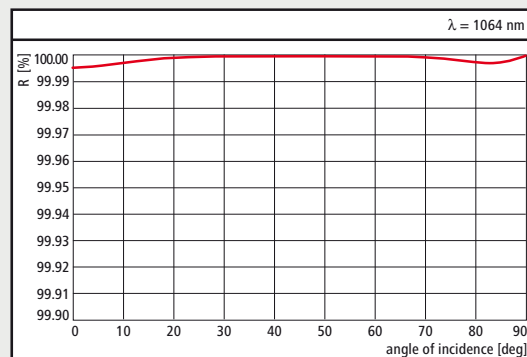


Figure 4: Reflectance vs. AOI of a wide angle scanning mirror for polarized Nd:YAG laser radiation:
HRs (0° – 90°, 1064 nm) > 99.9 %

These mirrors are ideal as scanning mirrors for s-polarized light or to enhance the reflectivity of optical gratings.

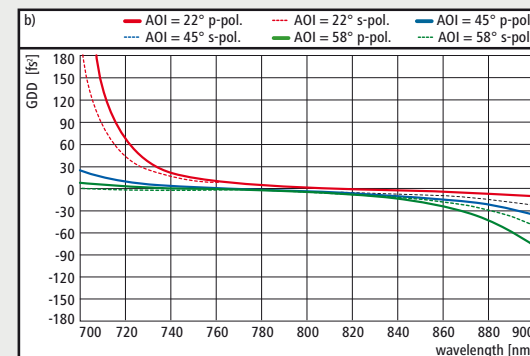
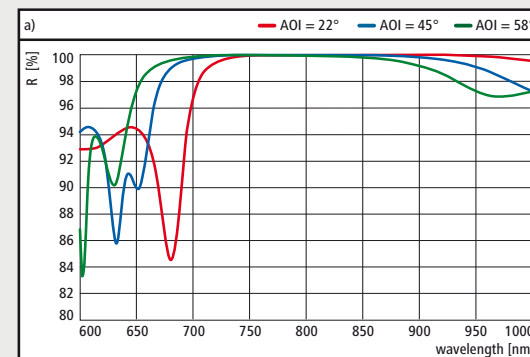
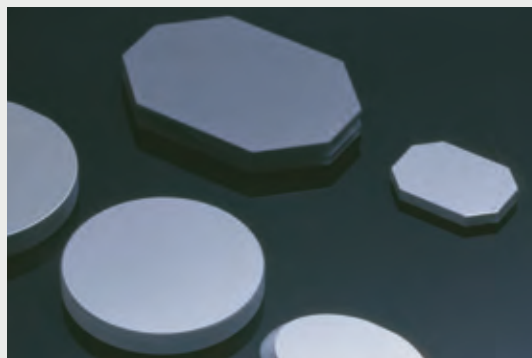


Figure 5: Reflectance and GDD spectra of a scanning mirror for femtosecond laser pulses from a Ti:Sapphire laser:
HRr (22° – 58°, 750 – 850 nm) > 99.5 %, |GDD| < 20 fs²
a) Reflectance vs. wavelength
b) GDD vs. wavelength

The broad low GDD wavelength range of these mirrors makes it possible to use them in femtosecond laser applications.

For more information or more examples on broadband and scanning mirrors please see pages 50 – 53 (optics for Ti:Sapphire and diode lasers), pages 74 and following (femtosecond laser optics) and, especially for scanning mirrors, page 120 – 121 (silver mirrors).

FILTERS FOR LASER APPLICATIONS

ANGLE TUNING OF NARROW BAND FILTERS

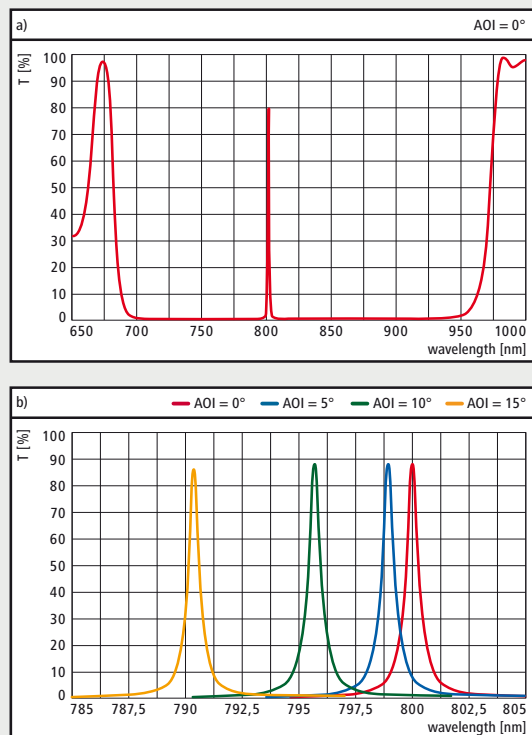


Figure 1: Transmission spectra of a narrow band filter for ~800 nm;
a) Transmission vs. wavelength, spectral overview
b) Transmission vs. wavelength at AOI = 0°, 5°, 10° and 15°

- Narrow band filters with FWHM of 1 nm and maximum transmission of $T > 80\%$.
- A FWHM of 50 pm with maximum transmission of $T = 50\%$ was demonstrated.
- Blocking: $T < 10^{-3}$; block band: ~200 nm in the Ti:Sapphire range.
- These filters are useful to select one wavelength from the spectrum of the Ti:Sapphire laser.

VARIABLE FILTERS FOR LASER APPLICATIONS

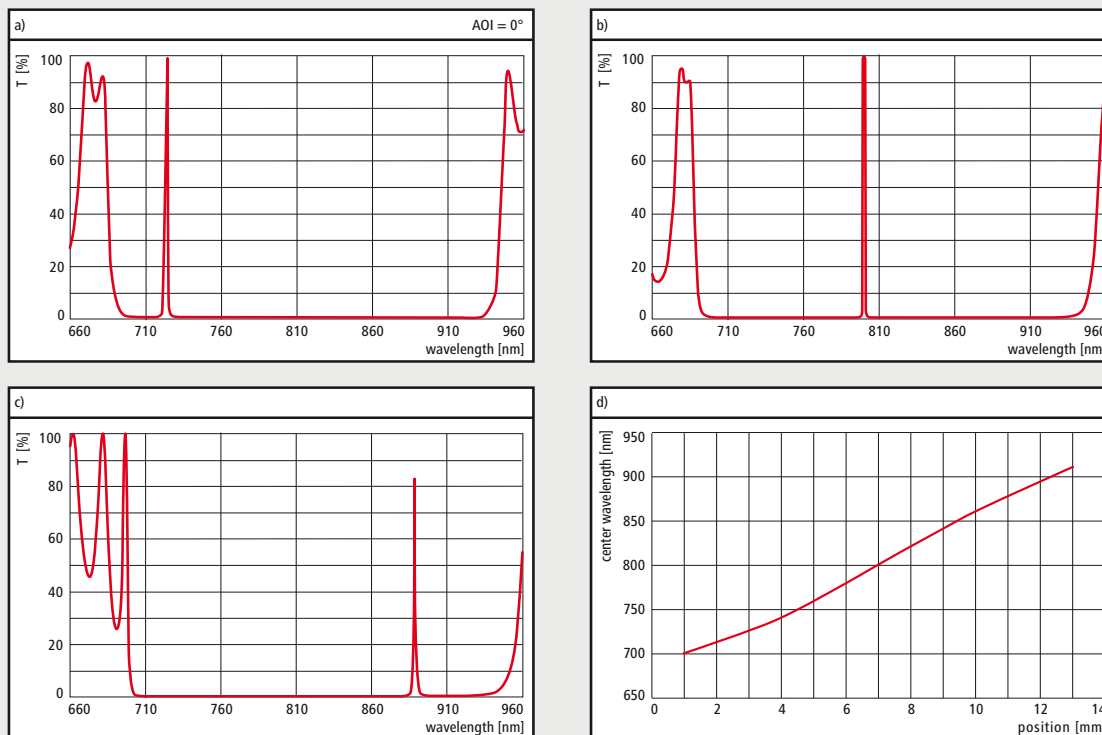


Figure 2: Transmittance spectra of a laterally variable filter for the wavelength range of the Ti:Sapphire laser taken
a) on the short wavelength side
b) in the center
c) on the long wavelength side of the filter
d) Center wavelength vs. position on the filter

Special features:

- Linear variation of the filter wavelength with the position on the filter.
- Similar designs for the VIS range (400 – 700 nm) and for the NIR range (up to 1800 nm).
- Blocking: $T < 10^{-3}$; block band: ~200 nm in the Ti:Sapphire range.
- Maximum transmittance: 90 %; FWHM: 1 nm.
- Shape: rectangular; size: 10 ... 20 mm long, 5 ... 10 mm wide.
- Spectral tolerance 1 % of center wavelength. The spectral position of the transmission band may vary by 1 % between the coating runs while the bandwidth remains unchanged. The spectral per-

formance of the filter can be optimized by tilting the filter. Tilting results in a shift of the transmission band towards shorter wavelengths. Thus, the spectral position of a filter, with the transmission band at longer wavelengths than required, can be adjusted for its best performance by angle tuning.

- If angle tuning is possible, the specifications for the filter can be less stringent which increases the output and reduces the price.

260 – 2500 nm

STEEP EDGE FILTERS

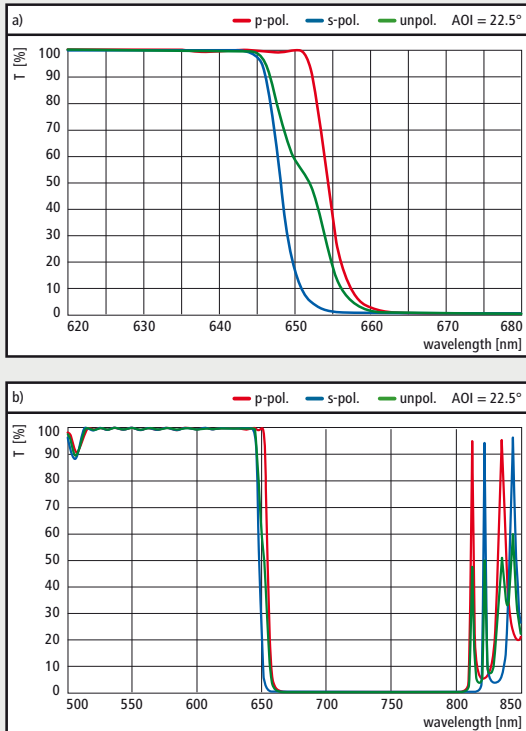


Figure 3: Transmission spectra of a steep edge short-wavelength pass filter for use as a combiner for laser diodes at 635 nm and 670 nm
 HRr (22.5°, 670 nm) > 99.9 %
 + HTr (22.5°, 635 nm) > 98 %, back side AR coated)
 a) Section around the edge of the blocking band
 b) Spectral overview

For more information on **combiners for diode lasers** see page 53.

For steep edge filters used as **pump mirrors** for solid-state lasers based on Yb-doped materials (e.g. Yb:YAG, Yb:KGW, Yb-doped fibers) see page 54.

NARROW BAND REFLECTANCE FILTERS

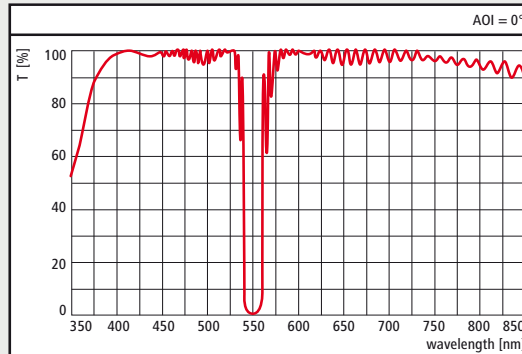


Figure 4: Transmittance spectrum of a narrowband reflectance filter for 550 nm

Filters of this type are ideal for the blocking of a single laser line while preserving a high and relatively constant transmission over the whole visible range.

Special features:

- Spectral width of the reflectance band: 3 % (e.g. $T < 1\%$ from 543 – 559 nm).
- $T < 0.1\%$ at the center wavelength.
- $T > 90\%$ throughout the visible spectral range.
- Filters for laser applications require excellent spectral quality and high damage thresholds.
- Spectral position of cut on/cut off wavelengths or reflectance bands according to customer specification.
- Sizes and shapes:

Edge filters can be produced on round or rectangular substrates up to diameters of 38.1 mm (1.5 inch). The production of miniature size filters (e.g. $3 \times 3 \text{ mm}^2$) is possible. Narrow band reflectance filters are limited to diameters of 25.4 mm (1 inch).

- Optical parameters are environmentally stable.

DUAL WAVELENGTH FILTER WITH BROAD BLOCKING RANGE

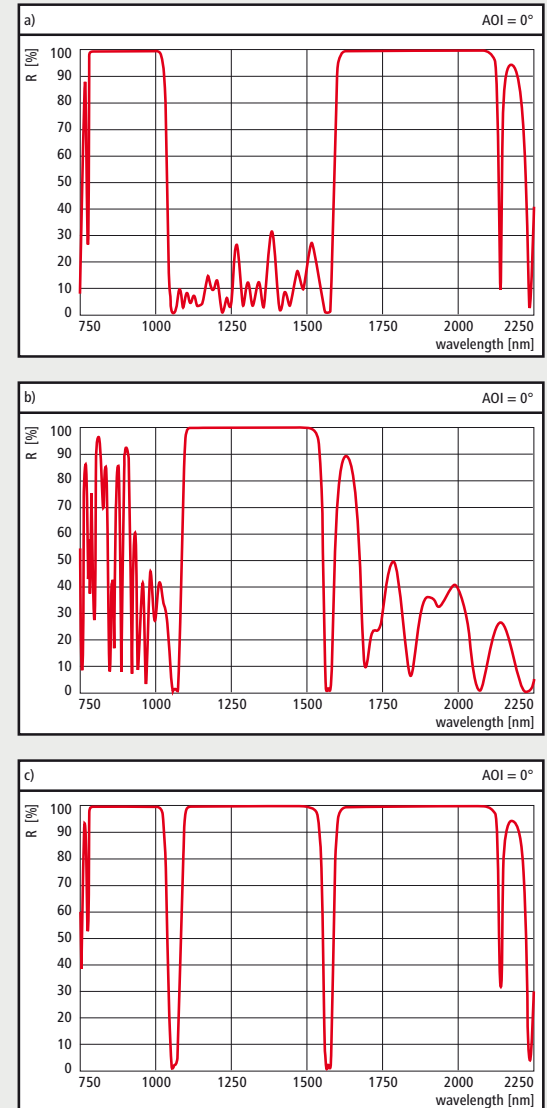


Figure 5: Reflectance spectra of a dual wavelength filter for 1064 nm and 1570 nm with a broadband blocking range from the UV to 2100 nm:

a) Front side coating

b) Back side coating

c) Sum

Double side coating reduces the mechanical stress. Blocking in the UV/VIS is done by a color glass.

THIN FILM POLARIZERS

TECHNICAL TERMS

First, we want to give the definitions of the most important technical terms to answer some frequently asked questions and to help our customers to specify thin film polarizers.

Light is a transversal wave; the vector of the electric field oscillates perpendicular with respect to the propagation direction of the light. Natural light (from the sun or from a lamp) is mostly "un-polarized" or "random polarized". This means that the oscillation planes of the electric field vectors of the single light waves are randomly distributed, but always transversal with respect to the direction of propagation. The term "linear polarized light" means, that there is only one plane of oscillation. There are different optics which can polarize light. An example of this would be crystal polarizers which split light into an un-polarized "ordinary beam" and a polarized "extraordinary beam" or thin film polarizers.

To explain the meaning of the terms "s-polarization" and "p-polarization" one must first determine a reference plane (see fig. 1). This plane is spanned by the incident beam and by the surface normal of the mirror (or polarizer). "**S-polarized light**" is the part of the light which oscillates perpendicularly to this reference plane ("**s**" comes from the German word "senkrecht" = perpendicular). "**P-polarized light**" is the part which oscillates parallel to the reference plane. Light waves with a plane of oscillation inclined to these directions can be described as a p-polarized and an s-polarized part.

The upper part of fig. 1 shows the reflectivity of a glass surface vs. AOI for s- and p-polarized light. The reflectivity for s-polarized light increases with

increasing angle of incidence. The reflectivity of p-polarized light decreases first by reaching $R = 0$ at the "Brewster angle", then increases for angles of incidence beyond Brewster angle. In principle, the same is true for dielectric mirrors. Thin film polarizers separate the s-polarized component of the light from the p-polarized component using the effect that the reflectivity for s-polarized light is higher and the reflection band is broader than for p-polarized light. There is always a wavelength range, where R_s is close to 100 % while R_p is close to zero. Special coating designs are used to make this wavelength range as broad as possible and to maximize the polarization ratio T_p/T_s . Very high values of T_p (> 99.5 %) can be measured very precisely using a special Cavity-Ring-Down setup. The TFP is inserted into a cavity thus introducing additional losses which are equal to $100\% - T_p$. One can also determine the most favorable AOI for each TFP by utilizing this method.

Thin film polarizers (TFPs) are key components in a wide variety of applications, e.g. in regenerative amplifiers. LAYERTEC produces thin film polarizers on plane substrates (dimensions according to customer specifications) for wavelengths between 260 nm and 2500 nm. All TFPs are optimized for high laser-induced damage thresholds. Although there is no certified measurement available, we know from several customers that the LIDT of a TFP is approximately one third of the LIDT of a high reflecting mirror for the same wavelength which is coated using the same technology.

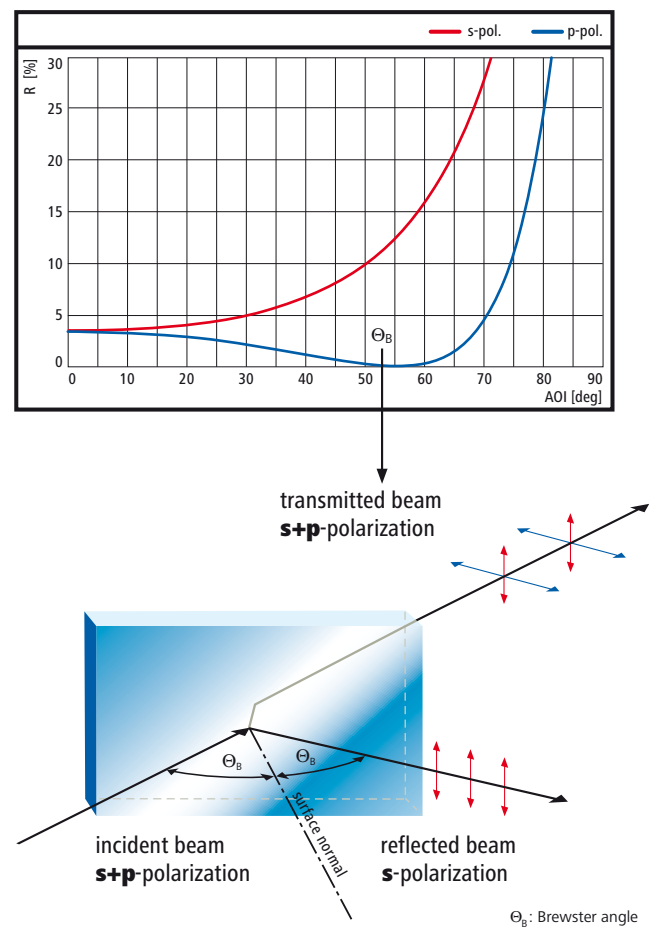


Figure 1: Explanation of the terms "s-polarized light" and "p-polarized light" and reflectance of an uncoated glass surface vs. angle of incidence for s- and p-polarized light

STANDARD THIN FILM POLARIZERS

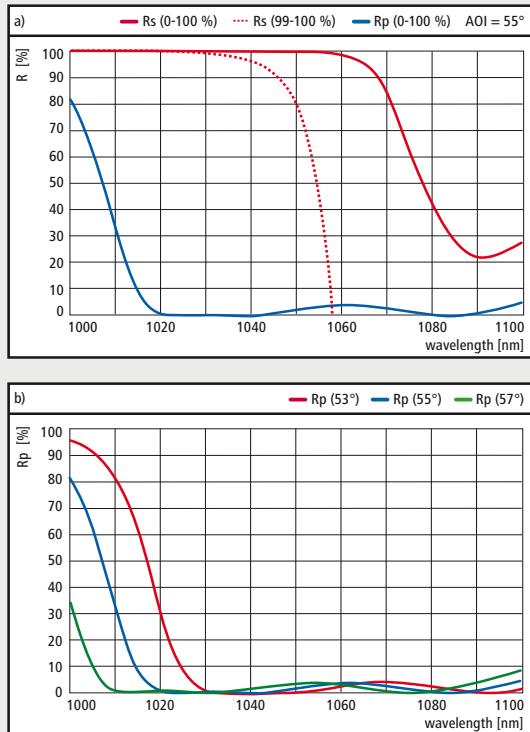
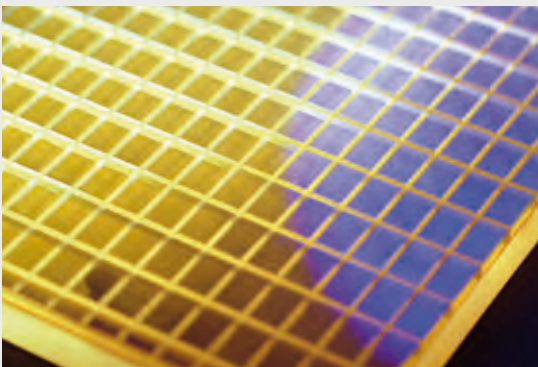


Figure 2: a) Reflectance spectra of a standard TFP for 1030 nm at $\text{AOI} = 55^\circ$ (Brewster angle) for s- and p-polarized light
b) Reflectance spectra of the same TFP design for $\text{AOI} = 53^\circ$, 55° and 57° for p-polarized light (angle tuning lowers R_p at 1030 nm from 0.25 % to < 0.1 % thus giving the chance to optimize the polarization ratio)



- TFPs can be produced for $\text{AOI} > 40^\circ$. Please note that thin film polarizers which work at the Brewster angle exhibit a considerably broader bandwidth and a higher T_p / T_s ratio than those which work at $\text{AOI} = 45^\circ$.
- Typical polarization ratios T_p / T_s : standard: > 500 ($\text{AOI} = 45^\circ$ or 55°).
- An extended wavelength range with a limited polarization ratio can be obtained by choosing AOI beyond Brewster angle.
- Special designs with a polarization ratio of T_p / T_s up to 10000 are possible.
- High laser-induced damage thresholds (useful for intracavity applications).
- It is favorable to design the laser so that the polarizers can be tilted by $\pm 2^\circ$ to adjust the polarizer for its best performance.
- The standard design can be applied for wavelengths between 260 nm and 2500 nm.

SPECIAL THIN FILM POLARIZERS

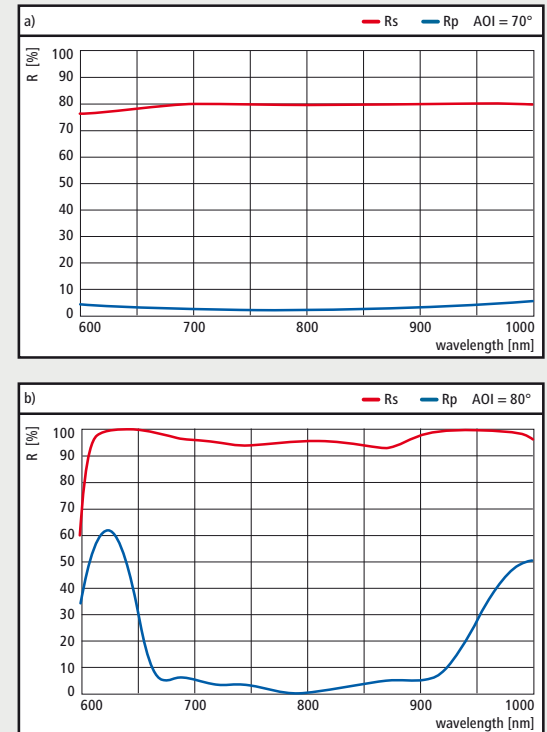


Figure 3: Broadband TFPs for the wavelength range of the Ti:Sapphire laser with different bandwidths and different polarization ratios, working at $\text{AOI} = 70^\circ$ and $\text{AOI} = 80^\circ$
a) R_p and R_s vs. wavelength, TFP designed for $\text{AOI} = 70^\circ$
b) R_p and R_s vs. wavelength, TFP designed for $\text{AOI} = 80^\circ$

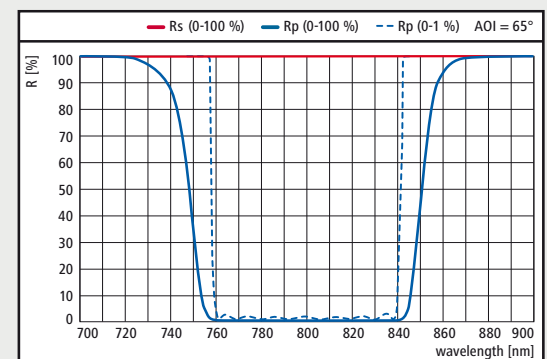


Figure 4: Broadband TFP for the 800 nm region

This special design provides an extremely broad polarizing wavelength range (~ 10 % of the center wavelength) with $T_p / T_s = 300 \dots 1000$.

LOW LOSS OPTICAL COMPONENTS

HR MIRRORS

- **R > 99.99 %** in the VIS and NIR spectral range
- **R > 99.999 %** was demonstrated at several wavelengths between 1000 ... 1600 nm.
- Mirrors with defined transmission (e.g. $T = 0.002 \%$).
- For Cavity Ring-Down time spectroscopy, it is favorable to adjust the transmission to the value of the scattering and absorption losses ($T = S + A$), see fig.1.
- All mirrors for CRD experiments are delivered with back side AR coating. Wedged substrates on request.
- Special polished plane and spherically curved fused silica substrates (see page 15).
- rms-roughness: $\leq 1.5 \text{ \AA}$.
- Surface quality: 10 - 5 scratch-digs, $5 / 1 \times 0.010$ (DIN EN ISO 10110).
- Coating technique: magnetron sputtering, ion beam sputtering.
- Optical parameters are stable against changes in temperature and humidity.
- Attractive prices for small and medium numbers of substrates per coating run.
- Very high reflectivity values for complex coating designs, e.g. GTI laser mirrors with $R > 99.95 \%$. (see pages 96 – 97)
- Vacuum packaging or packaging under nitrogen cover gas in dust free boxes.

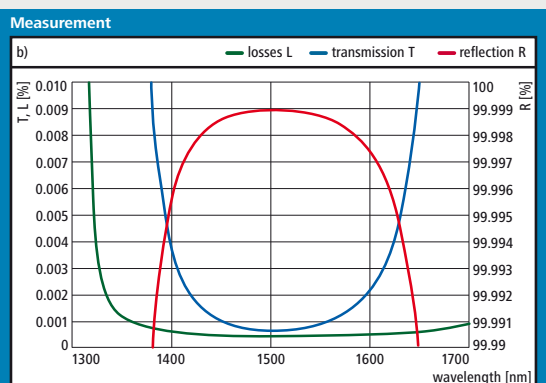
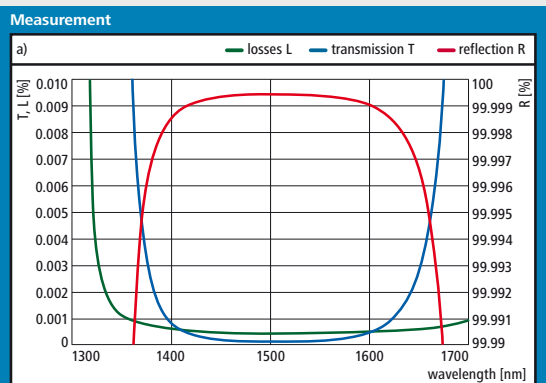


Figure 1: Reflectance, transmittance and loss spectra of low loss mirrors for 1550 nm

- a) Optimized for highest reflectance (transmission ~ 0)
b) Designed for $T \approx S + A$

Please note that the reflectivity of the mirrors in fig.1a and 1b is nearly the same. However, the extremely low transmission of the mirror in figure 1a makes CRD measurements very difficult.

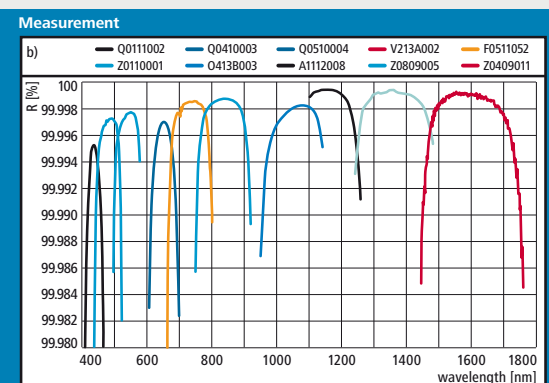
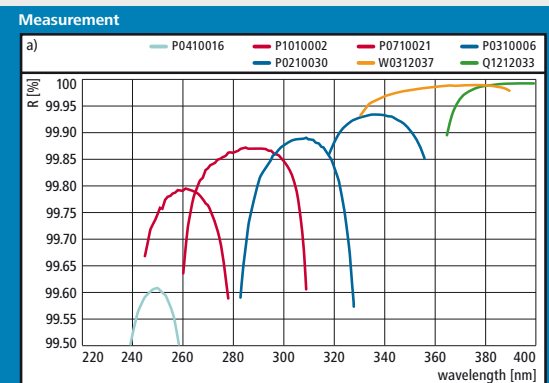


Figure 2: a) Reflectance spectra of a variety of low loss mirrors for the UV
b) Reflectance spectra of a variety of low loss mirrors for the VIS-NIR spectral range

All measurements were performed at the CRD setup which is described on pages 33 – 35. Please note that these mirrors are specially designed for relatively high transmission.

340 – 3000 nm

DIRECT MEASUREMENTS OF OPTICAL LOSSES

Type of losses	VIS	NIR
Scattering	Typical: 20 – 30 ppm Measured: 15 ppm @ 633 nm*, 20 – 30 ppm @ 532 nm**	< 10 ppm
Absorption	10 – 20 ppm***	< 10 ppm***
Total	< 50 ppm	< 20 ppm

* Measurement performed at Jenoptik L.O.S. GmbH, Jena
** Measurement performed at Fraunhofer Institute IOF Jena
*** Measurement performed at Leibniz-Institute of Photonic Technology (IPHT) e.V. Jena

CAVITY RING DOWN TIME MEASUREMENTS AND REFERENCE DATA

Wavelength	R _{max} [%]	T [%]	Loss [ppm] L = 1 - R - T	Measured at
248 nm	99.87	0.00024	1300	LAYERTEC GmbH
266 nm	99.941	0.0031	560	LAYERTEC GmbH
355 nm	99.988	0.0004	116	LAYERTEC GmbH
400 nm	99.9954	—	—	LAYERTEC GmbH
550 nm	99.9977	0.00039	19	LAYERTEC GmbH
633 nm	99.992	0.006	20	Westfälische Technische Hochschule Zwickau, Germany
660 nm	99.992	0.006	20	Universität Heidelberg, Germany
798 nm	99.995	0.003	10	LAYERTEC GmbH
840 nm	99.9988	0.0002	10	LAYERTEC GmbH
1030 nm	99.9980	0.0012	8	LAYERTEC GmbH
1150 nm	99.9994	0.00035	2.5	LAYERTEC GmbH
1392 nm	99.9985	0.0007	8	TIGER OPTICS, USA (R measurement) LAYERTEC GmbH (T measurement)
1550 nm	99.999	0.0002	8	IPHT Jena, Germany
2350 nm	99.995	0.002	30	University of Grenoble, France
3250 nm	99.928	0.012	600	University of Grenoble, France
4000 nm	99.9	—	—	Universität Bielefeld, Germany

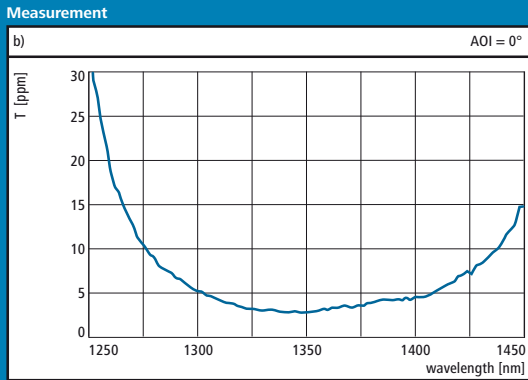
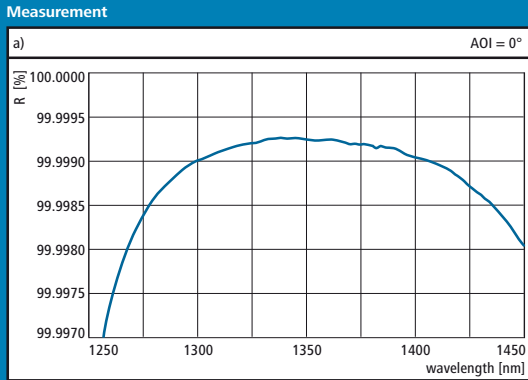


Figure 3: Measured reflectance and transmission spectrum of a low loss mirror for the wavelength range 1250 – 1450 nm
a) Reflectance vs. wavelength
b) Transmission vs. wavelength

Table 1: Reflectivity and transmission values of LAYERTEC low loss mirrors; Reflectance measured by Cavity Ring-Down spectroscopy, AOI = 0°

COATINGS ON CRYSTAL OPTICS

Laser applications using crystal optics have reached a high standard in industry and research. Optical coatings on crystals are an essential part of modern laser designs. They cover the wide range from single wavelength AR coatings on laser and nonlinear optical crystals up to complex multilayer coatings providing several high-reflectance and high-transmittance wavelength ranges and thus, replacing external laser mirrors.

LAYERTEC has a lot of experience in coatings on laser crystals. Our coatings are used in industrial high power Q-switched and cw lasers of several laser manufacturers. The quality of coatings on crystals depends on the coating technique as well as on the surface quality of the crystal. All coatings are produced by magnetron sputtering which guarantees very low stray light losses and a high environmental stability of the optical parameters.

The rapid progress in crystal growth techniques resulted in a wide variety of new crystals for laser applications, e.g. laser crystals like tungstanates and vanadates or nonlinear optical crystals like RTP. Each crystal type requires optimized polishing procedures and coating techniques. The coating design is determined by the optical properties of the crystal. However, the thermal expansion coefficients and the surface quality after storage and transport influence the coating quality as well. Especially, hygroscopic crystals like LBO or BBO require special pretreatments to achieve high damage thresholds and long lifetime for the coatings. Thus, coatings on new crystals always require experimental investigations to find the best coating procedures. Different dimensions and uncommon sizes and shapes are possible using the special LAYERTEC coating technology.

The following table gives an overview about the crystals which have already been coated at LAYERTEC and the types of layer systems which have been applied successfully.

Crystal Type	AR/BBAR	Single HR optional with HT	Double HR/BBHR optional with HT
a-SiO ₂	x	x	x
BBO	x		
BiBO	x	x	
CaCO ₃	x		
CTA	x		
Nd:GdVO ₄	x	x	x
Nd:GGG	x	x	
Nd:Cr:GSGG	x	x	
KTA	x	x	
KTP	x	x	x
Yb:KGW, Yb:KYW	x	x	x
LBO	x		
LiNbO ₃	x		
LMA	x		
Nd:LSB	x	x	x
RDP	x		
Ruby	x	x	
Ti:Sapphire	x	x	
Spinell	x	x	x
Cr:YAG	x	x	
Er:YAG	x	x	
Ho:YAG	x	x	
Nd:YAG, Yb:YAG	x	x	x
Nd:YALO (YAP)	x		
YLF	x	x	x
Nd:YVO ₄	x	x	x
ZGP	x		
ZnSe	x	x	

Every coating run will be performed with detailed measurement data sheets. Do not hesitate to contact us for a discussion or an offer on your special coating problem.

340 – 3000 nm

COATINGS ON DOPED LASER CRYSTALS

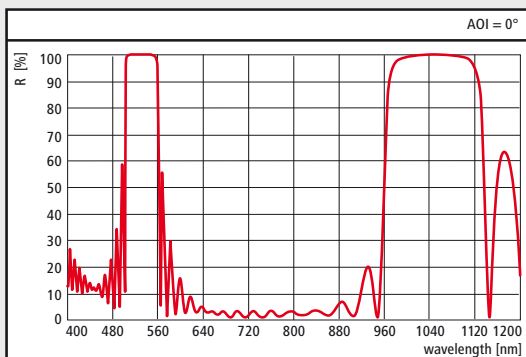


Figure 1: Reflectance spectrum of a dual HR mirror for 532 nm and 1064 nm with a HT region around 808 nm for pumping with a laser diode (on Nd:YAG)

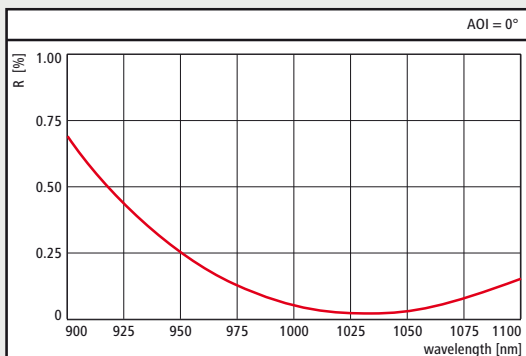


Figure 2: Reflectance spectrum of an AR coating for an Yb:KYW crystal:
AR (0°, 1030 nm) < 0.2 % + AR (0° - 30°, 980 nm) < 0.2 %.
Please note the large acceptance angle for the pump radiation

Sputtered coatings on laser rods, discs and slabs with:

- High laser-induced damage thresholds for critical industrial applications of Q-switched and cw lasers.
- Low residual reflectivity (e.g. $R < 0.1\%$ at 808 nm on Nd:YAG).
- Broadband and multiple wavelength AR coatings.
- Complex HR and HR / HT-coatings for compact laser designs (e.g. HR (532 nm) + HT (808 nm) on Nd:YVO₄ for diode pumped and frequency doubled "green" lasers).
- Coating of crystals with variable or special sizes and shapes.
- Coating of the full aperture of small crystals.

COATINGS ON NONLINEAR OPTICAL CRYSTALS

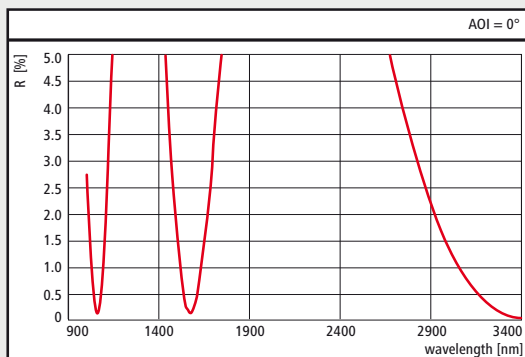


Figure 3: Reflectance spectrum of a triple wavelength AR coating on KTP:
AR (0°, 1064 nm + 1575 nm + 3400 nm) < 0.5 %

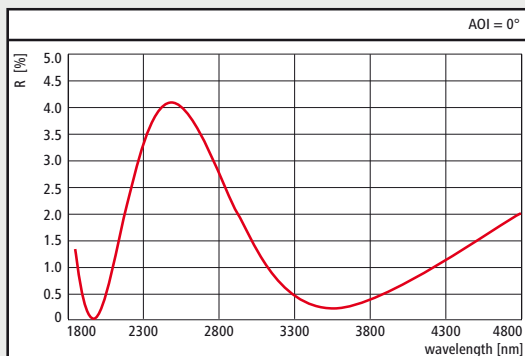


Figure 4: Reflectance spectrum of an AR coating for PPSLT:
AR (0°, 2000 nm) < 0.2 % + AR (0°, 3400 – 4400 nm) < 1.5 %

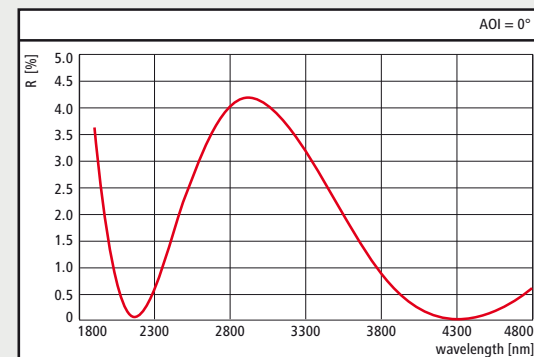


Figure 5: Reflectance spectrum of a dual wavelength AR coating on ZGP:
AR (0°, 2050 nm) < 1 % + AR (0°, 4300 nm) < 0.2 %

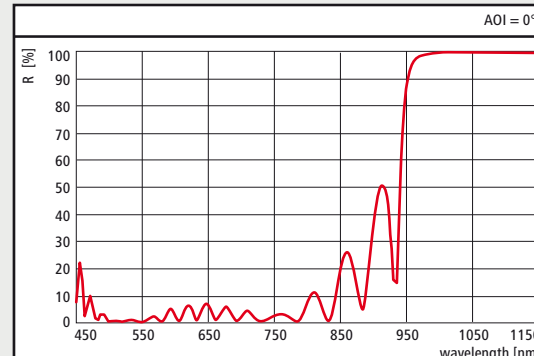


Figure 6: Reflectance spectrum of a dichroic mirror on KTP:
 $R(0^\circ, 532 \text{ nm}) < 1\%$ + $HR(0^\circ, 1064 \text{ nm}) > 99.95\%$

- Broadband and multiple wavelength AR coatings.
- Complex HR and HR / HT-coatings for compact laser designs, (e.g. HR (1064 nm) + HT (532 nm) on KTP for frequency doubled Nd:YAG or Nd:YVO₄ lasers).
- Coating of crystals with variable or special sizes and shapes.
- Coating of the full aperture on small crystals.

INTRODUCTION	PRECISION OPTICS	OPTICAL COATINGS	SELECTION OF OPTICAL COMPONENTS FOR COMMON LASER TYPES
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