CATALOG 2015





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INTRODUCTION	N,

PRECISION OPTICS

OPTICAL COATIN

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FEMTOSECOND LASER OPTICS	SELECTED SPECIAL COMPONENTS	METALLIC COATINGS FOR LASER AND ASTRONOMICAL APPLICATIONS
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PRECISION OPTICS



HOW TO SPECIFY SUBSTRATES

Price and quality of substrates are determined by material, shape, size, tolerances and polishing quality.

MATERIAL

The first decision is the material of the substrate. It should be free of absorption for all wavelengths of high transmission. If no transmission occurs, a low cost material can be used, e.g. Borofloat[®] (SCHOTT AG), for metallic mirrors.

With respect to the surface form tolerance, a low thermal expansion is beneficial.

SHAPE

The shape must be specified for both sides separately. Basically all combinations of plane, convex and concave surfaces are possible. A special role plays the wedge. A wedge (e.g. 30 arcmin) can be applied to any kind of surface (plane as well as convex or concave).

For curved substrates there are different conventions for the sign of the radius. Sometimes "+" means convex and "-" means concave. Other users refer "+" and "-" to the light propagation. In this case, "+" means "curvature with the direction of propagation" and "-" means "curvature against the direction of propagation". Please specify concave or convex in words or by the acronyms CC or CX to avoid confusion.

SIZE

The main decision should be about the size, i.e. the edge length or diameter. Small diameters are more favorable for the production. The sagitta heights become lower and it is easier to achieve a good form tolerance.

Although often specified otherwise in optical designs, the thickness description means the maximum thickness of the substrate, i.e. the center thickness for plano-convex substrates and the edge thickness for plano-concave substrates. Consequently, the thickness of a wedged plate is measured on the thicker side.



Figure 1: Conventions for the specification of the thickness of different types of substrates (schematic drawing)

In order to achieve a good form tolerance one should consider the ratio of diameter and thickness. As a rule of thumb the thickness should be the fifth of the diameter. Of course, other ratios are possible but the production cost and therefore the price increases.

TOLERANCES

Besides size and material, the tolerances are most important for manufacturing costs and therefore also for the price. Of course, the optics must fit into the mount, so that the diameter should not be larger than specified. The most common specification is \pm 0 - 0.1 mm. Mostly, the thickness is free in both directions. LAYERTEC usually specifies it with a tolerance of \pm 0.1 mm.

There is a lot of confusion about the specification of wedge, parallelism and centering. Please note that

wedge and parallelism describe the angle between the optical surfaces while centering describes the angle between the optical surfaces and the side surfaces (see fig. 2).





LAYERTEC standard substrates have a parallelism better than 5 arcmin. Specially made parallels may have a parallelism as low as < 10 arcsec. Standard wedged substrates have wedges of 0.5° or 1°. Larger wedge angles are possible depending on the substrate size.

Normally, the 90° angle to the side surface has a precision of 20 arcmin. Centering is an additional optics processing step which improves this accuracy to a few arcmin.

Using the same nomenclature, one can describe curved substrates. It should be distinguished between mirrors and lenses. The side surfaces of mirror substrates are just parallel. Nevertheless, the direction of the optical axis can be inclined to the side surfaces. After centering, the side surfaces are parallel to the optical axis. In that way, the mirror substrate becomes a lens.

SURFACE FORM TOLERANCE

The surface form tolerance is normally measured by interferometers and is specified in terms of lambda, which is the reference wavelength ($\lambda = 546$ nm if not otherwise stated). To avoid confusion, one must clearly distinguish between flatness, power and irregularity. In the following, flatness and irregularity shall be explained for a plane surface. Generally speaking, every real surface is more or less curved. Imagine that the "peaks" and "valleys" of a real surface are covered by parallel planes (see fig. 3). The distance between these planes is called the flatness. This flatness consists of two contributions. The first contribution is a spherical bend of the surface, which may be described by two best fitted spheres for the "peaks" and "valleys". With respect to an ideal plane, the sagitta of this curvature is denoted as power. This spherical bend does not affect the quality of the reflected beam. It just causes a finite focal length. The second contribution is the deviation of the best fitted spheres, which is named irregularity. This is the most important value for the quality of the beam.

The standard ISO 10110 provides a sufficient opportunity for specifying the surface form tolerance. Having the best comparability with the measurement results, all values are specified as numbers of interference fringes. They should be read as 1 fringe = $\lambda / 2$. In the drawings, the surface form tolerance is allocated as item number three:

 $\label{eq:approx} \begin{array}{l} 3 \ / \ power \ (irregularity) \\ \mbox{Example: A slightly bent } (\lambda \ / \ 4) \ optics \ which \ is \ regular \\ \ lar \ (\lambda \ / \ 10) \ would \ be \ specified \ as \ follows: \end{array}$

3/0.5 (0.2)

Using the optics only for transmission (e.g. laser windows), the power as well as the irregularity do not matter. An uprightly transmitted beam is not affected if the optics has the same thickness all over the free aperture. The deviation from this equality is defined in a similar way as the flatness. It is also measured in parts of the reference wavelength and called "transmitted wave front". For instance, the window in fig. 3c has a flatness of λ /4 but a transmitted wave front of λ /10.

COATING STRESS

Thin substrates cannot withstand the coating stress. The coating will cause a spherical deformation. This means that a finite sagitta or power occurs. In case of circular substrates, the irregularity is not affected by this issue.

The flatness becomes poor when seriously considering the mentioned values. Nevertheless, the quality of a normally incident beam is not affected.

DEFECTS

MIL-O-13830 and ISO 10110 are different standards for the description of optical elements. This often causes obscurities. Basically, one should distinguish between scratches and digs. The scratch number in MIL-O-13830 means the visibility of the biggest scratch compared to the corresponding one on a norm template. Actually "10" is the smallest scratch on this template. Thus, better qualities cannot be specified seriously. The MIL norm does not specify a directly measured scratch width. Sometimes the number is interpreted as tenths of a micron, sometimes as microns. Actually, a direct measurement never corresponds to the MIL norm.

In contrast to the scratch, the dig number can be measured easily. The numerical value means the maximum dig diameter in hundredths of a millimeter. Maximum size digs can be one per 20 mm of diameter. According to ISO 10110 the defects are specified as item number 5. The grade number means the side length in millimeters of a quadratic area which is equivalent to the total fault area. So, $5 / 1 \times 0.025$ means a surface fault area of 0.000625 mm^2 . Additionally, scratches of any length are denoted with a leading L. A long scratch with a width of 4 microns would be specified as L 1 x 0.004.

All these explanations are very simplified. For a detailed specification please read the complete text of the relevant standard.

PLEASE NOTE:

There is no direct conversion between MIL-O-13830 and ISO 10110. All specifications in this catalog correspond to ISO 10110. The mentioned scratch/dig values are a rough analog to MIL-O-13830.

Figure 3: Schematic drawing for the explanation of substrate properties: a) Flatness of $\lambda/10$

b) Spherical bending (power of $\lambda/4$)

c) Irregularity of $\lambda/4$, but transmitted wavefront of $\lambda/10$



STANDARD QUALITY SUBSTRATES

The precision optics facility of LAYERTEC produces plane and spherical curved mirror substrates, lenses and prisms of fused silica, optical glasses like N-BK7[®] and SF14[®] and some crystalline materials, e.g. calcium fluoride and YAG. In the following you can find information on the specifications of our standard substrates.

Please do not hesitate to contact us also for other sizes, shapes, radii and materials or for special components.

STANDARD SPECIFICATIONS

Materials

- Fused silica: Corning 7980[®] or equivalent
- Fused silica for high power applications: Suprasil[®] 300 / 3001 / 3002 or equivalent
- UV fused silica (excimer grade): SQ1 E-193[®] and SQ1 E-248[®]
- IR fused silica: Infrasil 302[®] or equivalent
- ULE[®]
- Zerodur[®]
- N-BK7[®] or equivalent
- CaF₂:

single crystal, random oriented, special orientations on request, excimer grade (248 nm and 193 nm) on request

- Sapphire: single crystal, random oriented, special orientations on request
- YAG:
 - undoped, single crystal, random oriented

All trademarks mentioned are the property of the respective owners.

Plane substrates, parallels and wedges

- Standard plane substrates: wedge < 5 arcmin
- Standard parallels:

wedge < 1 arcmin or wedge < 10 arcsec

 Standard wedges: wedge = 30 arcmin or wedge = 1 deg

Plano-concave and plano-convex substrates

Standard radii:
25, 30, 38, 50, 75, 100, 150, 200, 250, 300, 400, 500, 600, 750, 1000, 2000, 3000, 4000, 5000 mm

Dimensions

- Fused silica, ULE[®], Zerodur[®], N-BK7[®]: diameter 6.35 mm ... 508 mm (¼ inch ... 20 inches)
- Calcium fluoride, YAG, sapphire: diameter 6.35 mm ... 50.8 mm (1/4 inch ... 2 inches)
- Rectangular substrates and other diameters available on request

Tolerances

- Diameter:
- + 0 mm, 0.1 mm • Thickness:
- ± 0.1 mm
- Clear aperture: central 85 % of dimension
- Chamfer:
 0.2 ... 0.4 mm at 45°









Ø: Diameter [mm] t.: Edge thickness [mm] t.: Center thickness [mm] t: Thickness [mm]

FEMTOSECOND LASER OPTICS	SELECTED SPECIAL COMPONENTS	METALLIC COATINGS FOR LASER AND ASTRONOMICAL APPLICATIONS
	SELECTED STECKE CONTROLLETS	

Surface form tolerance (reference wavelength: 633nm)

Material		Standard Specification	On request
Fused silica	plane	$\lambda/10$	λ/30
	spherical	$\lambda/4$ reg. (typical $\lambda/10$ reg.)	λ/30 reg. (Ø<51 mm)
ULE [®] and Zerodur [®]	plane	$\lambda/10$	λ/30
	spherical	$\lambda/4$ (typical $\lambda/10$ reg.)	λ/30 reg. (Ø<51 mm)
N-BK7®	plane	$\lambda/10$	λ/30
	spherical	$\lambda/4$ reg. (typical $\lambda/10$ reg.)	λ/30 reg. (Ø<51 mm)
CaF ₂	plane Ø < 26 mm	$\lambda/10$	λ/20
	plane Ø < 51 mm	$\lambda/4$	λ/20
	spherical	$\lambda/4$ reg.	λ/20 reg.
Sapphire		λ/2	λ/30
YAG	plane	$\lambda/10$	λ/30
	spherical	$\lambda/4$ reg. (typical $\lambda/10$ reg.)	λ/30 reg. (Ø<51 mm)
Si	plane	$\lambda/10$	λ/20
	spherical	$\lambda/4$ reg. (typical $\lambda/10$ reg.)	λ/20 reg. (Ø < 51 mm)

Surface quality

Material	Standard Roughness	Standard Specification	On request		
Fused silica	< 2 Å	5 / 1 x 0.025 L1 x 0.001 Scratch-Dig 10-3	< 1.2 Å	5 / 1 x 0.010 L1 x 0.0005 Scratch-Dig 5-1	
ULE®	< 2 Å	5 / 3 x 0.025 L1 x 0.001 Scratch-Dig 10-5	< 2 Å	5 / 1 x 0.010 L1 x 0.0005 Scratch-Dig 5-1	
Zerodur®	< 4 Å	5 / 2 x 0.040 L1 x 0.001 Scratch-Dig 10-5	< 3 Å	5 / 2 x 0.025 L1 x 0.0010 Scratch-Dig 10-3	
N-BK7®	< 3 Å	5 / 2 x 0.040 L1 x 0.001 Scratch-Dig 10-5	< 3 Å	5 / 2 x 0.025 L1 x 0.0010 Scratch-Dig 10-3	
CaF ₂	< 4 Å	5 / 3 x 0.025 L1 x 0.0025 Scratch-Dig 20-3	< 1.5 Å	5 / 3 x 0.016 L1 x 0.0010 Scratch-Dig 10-2	
Sapphire	< 5 Å	5 / 3 x 0.025 L20 x 0.0025 Scratch-Dig 20-3	< 3 Å	5/3 x 0.016 L1 x 0.0010 Scratch-Dig 10-2	
YAG	< 3 Å	5 / 1 x 0.025 L2 x 0.0025 Scratch-Dig 20-3	< 3 Å	5 / 1 x 0.010 L1 x 0.0005 Scratch-Dig 5-1	
Si	< 3 Å	5 / 3 x 0.025 L1 x 0.001 Scratch-Dig 10-5	< 2 Å	5 / 1 x 0.010 L3 x 0.0005 Scratch-Dig 5-1	

All specifications according to ISO 10110 (Ø 25 mm). The mentioned Scratch-Dig values are approximately equivalent to MIL-O-13830

ASPHERES, OFF-AXIS AND FREE FORM OPTICS

BASICS

Plane and spherical optics can be efficiently manufactured by using traditional techniques of area grinding and polishing. The tool always works on a significant fraction of the substrate area at once. It is not or hardly possible to manufacture surface geometries that differ from regular forms like planes, spheres or cylinders.

Using ultra precision CNC machinery, surfaces can be zonally processed, i.e. the tool works on one point at a time. The possible surface forms and tolerances are only limited by the precision of the machine and the measurement equipment. In contrast to the areal techniques, zonal processing usually works with one single piece per run only.

The non-spherical optics can be divided in three groups: rotational symmetric non-spherical, off-axis and free form optics.



Figure 1: Aspheric lens

ROTATIONAL SYMMETRIC NON SPHERICAL OPTICS (ASPHERES)

Although the term "asphere" may stand for any nonspherical optics, it is often referenced to rotationally symmetric non-spherical optics. They are described by the following equation (ISO 10110):

$$z(r) = \frac{r^2}{R \left[1 + \sqrt{1 - (1 + k) \frac{r^2}{R^2}}\right]} + A_4 r^4 + A_6 r^6 + \dots$$

- z = displacement
- k = conic constant
- r = distance from axis
- R = radius of curvature
- A_{i} = aspheric coefficients

Neglecting the aspheric coefficients leads to a profile of conic sections:

- Ellipse: -1 < k < 0
- Sphere: k = 0
- Parabola: k = -1



Figure 2: Profile of an aspheric mirror

	Dimension	Tolerances
Total diameter	25 560 mm	< 0.1 mm
Inspection range	< 550 mm	
Total thickness	< 100 mm	< 0.1 mm
Displacement	< 50 mm	
Centering error		< 50 µm
Tilting error		< 30 ''
Surface form tolerance		$< \lambda/4$ (< $\lambda/10$ on request)
Roughness		< 3 Å

Table 1: Production dimensions and tolerances

OFF-AXIS SURFACES

An off-axis surface can be seen as a section of a bigger on-axis surface. The focal point still is on the original optical axis but not the center of the section. It is located off axis.

Off-axis surfaces derived from aspheres are described by the mentioned equation, the off-axis distance a and / or the off-axis angle α .

Examples:

- Off-axis parabolas
- Off-axis ellipses
- Off-axis hyperbolas
- Off-axis spheres
- Off-axis cylinders

Example: Off-Axis Parabola (OAP)



Figure 3: Schematic drawing of an off-axis parabola

The focal length of the parent parabola (parent focal length) is measured from the vertex on the optical axis. For the off-axis parabola, an effective focal length $f_{\rm eff}$ is introduced.

The off-axis distance is measured from the optical axis to the middle of the OAP. The radius R denotes the radius of curvature in the vertex of the parent parabola. The conic constant k is -1.

Free form surfaces are always customer specific,

defined by a number of points or equations. No

symmetry may be assumed. Free form surfaces are

Table 2 shows LAYERTEC's production dimensions

FREE FORM SURFACES

manufactured as single pieces.

and tolerances for free form surfaces.

In principle an off-axis substrate can always be mechanically cut from an on-axis substrate. The alternative way is a direct manufacturing. Depending on the size and tolerances, both ways are possible. Fig. 4 shows the common process of manufacturing a number of smaller OAPs from a parent parabola.





Figure 4: Manufacturing off-axis parabolas as pieces of one "parent parabola"

Figure 5: Basic properties of a free form substrate

	Dimension	Tolerances
Ø	< 300 mm	0.2 mm
b	< 300 mm	0.1 mm
c	< 450 mm	0.1 mm
α	< 45°	
t	< 80 mm	0.1 mm
а		
Surface form tolerance		$< \lambda/2$ ($\lambda/4$ on request)
Roughness		< 3 Å

Table 2: Dimensions and tolerances of free form substrates

MATERIALS

The surface quality and the final tolerances depend very strongly on the material of the substrate. LAYERTEC has an optimized process for fused silica.

Materials like Zerodur[®], ULE[®] or N-BK7[®] may be used in special cases.

MEASUREMENT

Measuring aspheric surfaces requires sophisticated devices. LAYERTEC applies 4 different measurement principles.

• Tactile measuring

The tip has mechanical contact to the surface and its excursion is recorded. It measures one line at a time. Precision < 200 nm on a 200 mm line.

- Single point interferometer
 Contactless measurement of the surface, measuring the surface point by point. Precision < 50 nm on a diameter of 420 mm.
- Interferometer with reference surface It compares the surface to a well-known reference surface. Precision < 50 nm, diameter 300 mm. Concave surfaces preferred.
- Interferometer with hologram
 It compares the surface to the wave front which is
 generated by a computer generated hologram (CGH).



Figure 6: LuphoScan single point interferometer

SPECIAL OPTICAL COMPONENTS

ETALONS

As a kind of a Fabry-Pérot interferometer, the etalon is typically made of a transparent plate with two reflective surfaces. Its transmission spectrum, as a function of wavelength, exhibits peaks of high transmission corresponding to resonances of the etalon. Etalons are widely used in telecommunication, lasers and spectroscopy for controlling and measuring the wavelength of laser sources. LAYERTEC offers etalons of customized diameters and various materials depending on the wavelength range. Thicknesses down to 50 μ m and a parallelism < 1 arcsec are possible subject to the diameter. Do not hesitate to contact us for the customized diameter and thickness you need.

	Ø = 50 mm	Ø = 25 mm	Ø = 12.7 mm	Parallelism	
Fused Silica	≥ 200 µm	≥ 130 µm	≥ 50 µm	< 1 arcsec	
YAG	≥ 200 µm	≥ 130 µm	≥ 50 µm	< 1 arcsec	
CaF ₂		≥ 300 µm	≥ 100 µm	< 5 arcsec	

WAVEPLATES

LAYERTEC offers customer specific retardation plates made of crystalline quartz. Due to the minimal required thickness the below mentioned wave plates are available:

Order	Ø = 38 mm	Ø = 25 mm	Ø = 12.7 mm	Precision	Parallelism			
λ/2	Available wavelengths							
K = 0			$\lambda = 900 \text{ nm}$	± 1 μm	< 1 arcsec			
K = 1	$\lambda = 900 \text{ nm}$	$\lambda = 800 \text{ nm}$	$\lambda = 350 \text{ nm}$	± 1 μm	< 1 arcsec			
K = 2	$\lambda = 550 \text{ nm}$	$\lambda = 500 \text{ nm}$	$\lambda = 300 \text{ nm}$	± 1 μm	< 1 arcsec			
λ/4	Available wavelengths							
K = 1	$\lambda = 1060 \text{ nm}$	$\lambda = 940 \text{ nm}$	$\lambda = 400 \text{ nm}$	± 1 μm	< 1 arcsec			
K = 2	$\lambda = 620 \text{ nm}$	$\lambda = 530 \text{ nm}$	$\lambda = 300 \text{ nm}$	± 1 μm	< 1 arcsec			

CUSTOMIZED PRISMS AND SHAPES

In addition to the mentioned circular substrates, LAYERTEC is able to produce a lot of different shapes. Uncommon optics are possible besides rectangular substrates, wedges and prisms. Typical examples of uncommon optics are defined holes through the optics. So-called D-cuts and notches can be produced.

POLISHING OF CRYSTALS

Besides the high quality optical coatings on crystals (see pages 116, 117), LAYERTEC supports the polishing of various types of crystals such as YAG, KGW, KYW, ZGP or LBO. Our polishing technology also enables the careful handling and processing of small crystal sizes or extraordinary forms. Do not hesitate to contact us for your special problem.

LARGE SCALE OPTICS

LAYERTEC has established a production line for plane and spherical optics up to a diameter of 500 mm. This also includes interferometers. Measurements for large optics are described on page 22. The optics can be coated using magnetron sputtering and IAD. The main products are large scale laser mirrors. A coating uniformity of ± 0.5 % was demonstrated which also enables the production of large scale thin film polarizers and other complex coating designs.



Figure 1: Mirror substrate with a diameter of 500 mm

SUBSTRATE MATERIALS FOR UV, VIS AND NIR/IR OPTICS

	YAG (undoped)	Sapphire	BaF ₂	CaF ₂	Infrasil ^{®1)}	Fused silica (UV)	N-BK7 ^{®2)}	SF10 ^{®2)}
Wavelength range free of absorption	400 nm – 4 μm	400 nm – 4 μm	400 nm – 10 μm	130 nm – 7 μm	300 nm – 3 μm	190 nm – 2.0 μm³)	400 nm – 1.8 μm	400 nm – 2.0 μm
Refractive index at								
200 nm				1.49516		1.55051		
300 nm				1.45403		1.48779		
500 nm	1.8450	1.775	1.479	1.43648	1.46233	1.46243	1.5214	1.7432
1 µm	1.8197	1.756	1.468	1.42888	1.45042	1.45051	1.5075	1.7039
3 µm	1.7855	1.71	1.461	1.41785	1.41941			
5 μm		1.624	1.451	1.39896				
9 μm			1.408	1.32677				
Absorbing in the 3 µm region	no	no	no	no	yes	yes	yes	yes
Absorbing in the 940 nm region	For high powe	er applications a	it 940 nm we re	commend the f	used silica type	s SUPRASIL 300®	ⁱ⁾ and SUPRASIL	3001/3002 ^{®1)}
Birefringence	no	yes	no	no ⁴⁾	no	no	no	no
Thermal expansion coefficient [10 ⁻⁶ K] ⁵⁾	7	5	19	18	0.5	0.5	7	8
Resistance against temperature gradients and thermal shock	high	high	very low	low	high	high	medium	medium
GDD fs ² per mm								
400 nm	240	150	90	68	98	98	120	640
800 nm	97	58	38	28	36	36	45	160
1064 nm	61	29	26	17	16	16	22	100
1500 nm	13	-25	13	1.9	-22	-22	-19	38
2000 nm	-59	-120	-2.4	-21	-100	-100	-99	-36
TOD fs ³ per mm								
400 nm	75	47	27	19	30	30	41	500
800 nm	57	42	20	16	27	27	32	100
1064 nm	71	65	22	21	44	44	49	100
1500 nm	140	180	34	46	130	130	140	140
2000 nm	360	530	72	120	450	450	460	350

¹⁾ Registered trademark of Heraeus Quarzglas GmbH & Co. KG

²⁾ Registered trademark of SCHOTT AG

inconsistent. Please note that the thermal expansion coefficient of crystals depends also on the crystal orientation.

³ Absorption band within this wavelength range, please see transmission curve
 ⁴ Measurable effects only in the VUV wavelength range

All values are for informational purposes only. LAYERTEC cannot guarantee the correctness of the values given.

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⁵⁾ The values given here are rounded, because the measurements of different authors in the literature are

TRANSMISSION CURVES





MEASUREMENT TOOLS FOR PRECISION OPTICS

SURFACE FORM MEASUREMENT

For the measurement of surface form and regularity, the precision optics facility of LAYERTEC is equipped with laser interferometers and special interferometer setups for plane, spherical and parabolic surfaces. Additionally, a tactile measurement device (Taylor Hobson PGI 1240 Asphere) is available for general aspheric and grinded surfaces. Besides the purpose of quality control, surface form measurement is a key function for the zonal polishing technology established at LAYERTEC.

Abbreviations

- **P-V:** The peak-to valley height difference
- **ROC:** Radius of curvature of a spherically curved surface.
- λ: measuring wavelength of the laser interferometer (e.g. 633 nm or 546 nm). The P-V value is stated in a fractional amount of λ. The concrete value of λ is stated in our protocols.

For detailed information about the standards concerning surface form measurement please refer to ISO 10110-5.

Accuracy of interferometric measurements

Without special calibration procedures, the accuracy of an interferometric measurement is only as accurate as the reference surface. Calibration can increase the accuracy by a factor of 2 or more. Furthermore, the precision is influenced by the size of the measured area and in case of a curved surface by the radius of curvature itself. The accuracy values stated as "P-V better than ..." in the following articles are guaranteed values. Very often accuracies of $\lambda/20$ or better will be achieved.

Standard measurements

In general, the form tolerance of spherical and plane optics with diameters $\emptyset \le 100$ mm can be measured with an accuracy of P-V better than $\lambda/10$ by using

ZYGO Fizeau interferometers. To cover a measurement range of ROC = \pm 1200 mm over an aperture of \emptyset = 100 mm, LAYERTEC uses high precision JenFIZAR Fizeau objectives. In many cases, a higher accuracy up to P-V = λ /30 is possible. Measurement protocols can be provided on request.

Large Radius Test (LRT)

Surfaces with radii of curvature beyond \pm 1200 mm are tested with a special Fizeau zoom lens setup called Large Radius Test (LRT). This setup was developed by DIOPTIC GmbH in cooperation with LAYERTEC.

Its operating range is ROC = \pm 1000 mm ... \pm 20.000 mm at working distances lower than 500 mm. The accuracy is guaranteed as P-V = $\lambda/8$ over $\emptyset \le 100$ mm, but typically it is better than P-V = $\lambda/15$. LRT has the advantages that only one Fizeau-objective is needed to cover a wide range of radii of curvature and that the working distance is kept small. This reduces the influence of disturbing air turbulences during the measurement.

Large aperture interferometry

LAYERTEC uses high performance interferometers especially for laser optics with large dimensions. A wavelength-shifting Fizeau interferometer (ADE Phaseshift MiniFIZ 300[®]) is used for flat surfaces. LAYERTEC has enlarged the measurement aperture of the system with a special stitching setup. The measurement range of the system is:

- P-V up to λ / 50 (633 nm) at Ø \leq 300 mm with a full aperture measurement
- P-V better than $\lambda/10$ (633 nm) at $\emptyset \le 600$ mm with a special stitching measurement setup.

Figure 1 shows the height map of a flat surface with diameter of \emptyset = 520 mm which was measured with the MiniFIZ 300 interferometer and the stitching configuration at LAYERTEC.

The measurements of spherical concave surfaces are made with a Twyman-Green interferometer (Phase-Cam 5030®; 4D-Technology). This interferometer uses a special technology which allows measurement times in the region of a few milliseconds. Therefore, the interferometer is insensitive to vibrational errors when measuring over long distances up to 20 m between the device and the specimen. The measurement accuracy of the system is P-V better than $\lambda / 10$ at $\emptyset \leq 600$ mm with a full aperture measurement (in case of concave surfaces).



Figure 1: Height map of a flat surface with a diameter of \emptyset = 520 mm polished and measured at LAYERTEC. The P-V value is λ / 10 over the full aperture (\emptyset = 500 mm inspection area) after zonal correction.

SURFACE ROUGHNESS MEASUREMENT

The surface roughness value of an optical surface is denoted as roughness parameter Rq or Sq. This parameter is also named "RMS roughness" because it is calculated as the root mean square of the surface height values. The letter "R" indicates that only a two-dimensional roughness profile is the basis of the calculation according to ISO 4287-1. The letter "S" means a three-dimensional measurement and calculation (3D-Reference ISO 25178-2).

The corresponding measurement device and the spectral range within which the optical surface should be used have to be taken into account when measuring and stating roughness parameters of optical surfaces. The spatial resolution of the roughness measurement device plays an important role with respect to the roughness value. A higher spatial resolution allows the detection of smaller surface structures and higher spatial frequencies. Furthermore, the amount of stray light losses on the surface depends on the spatial frequencies of the surface structures and the wavelength of the light itself. Fig. 2 shows the spatial frequencies which influence the scattering losses in different spectral ranges and typical spatial resolutions of roughness measurement devices.



Figure 2: Spatial frequency resolution of AFM and 3D optical surface profiler at LAYERTEC for typical scan sizes. Additionally, the figure shows the spatial frequency ranges which influence the scattering losses in the VIS and DUV spectral range*.

Generally, for the characterization of optical surfaces which are appointed to be used in the NIR, VIS and UV spectral range, surface roughness measurements should be accomplished with spatial resolutions which are equal or better than 10 / µm to obtain roughness information over the entire relevant spatial frequency range. Fig. 3 clarifies the differences between an AFM measurement and an optical surface profiler measurement with respect to the calculated RMS roughness and the spatial resolution.



LAYERTEC has available a phase shifting three-dimensional optical surface profiler (Sensofar) and a scanning probe microscope (AFM) DI Nanoscope 3100 for the purpose of measuring and analyzing the surface roughness of optical components. The optical profiler provides a low spatial resolution $< 2 / \mu m$ combined with an acquisition time of only a few seconds. The device is used for the measurement of optics with lower surface roughness requirements and for the general inspection of the polishing processes. Surface defects and inhomogeneities can be characterized too. The AFM is used for the characterization of polished surfaces with roughness values Sq < 0.5 nm. This device has a very high spatial resolution horizontally and vertically, but the acquisition time is approximately 10 - 30 minutes. Therefore, it is primarily used for the further development of the polishing processes. Our premium polishing process and especially our optics for UV applications with Sq. <0.2nm are checked periodically for quality control reasons. The standard AFM measurement parameters at LAYERTEC are: Scan size of 10 x 10 µm² and a spatial resolution of 25 / µm (see fig. 2). Measurement reports are available on request.

 For more information on stray light losses please see: A. Duparré, "Light scattering on thin dielectric films" in "Thin films for optical coatings", eds. R. Hummel and K. Günther, p. 273 – 303, CRC Press, Boca Raton, 1995.

Figure 3: Surface roughness measurement of a super polished Low Loss substrate for an UV application made of fused silica. Both images show the same region on the surface, but they were recorded with different measurement devices (optical surface profiler and AFM). The color bar scaling is ± 1 nm for both images. With equivalent lateral pixel scaling, the AFM measurement with high spatial resolution shows fine structures which are relevant for stray light losses. The optical profiler measurement only shows a few pixels but no significant information about the surface roughness and structures. Therefore, undersampling yields better roughness values and overstates the surface quality.

